

JC13 Rec'd PCT/PTO 27 MAR 2002

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| FORM PTO-1390 (REV 10-2000) | | U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE | | ATTORNEY'S DOCKET NUMBER P/25-277 | |
| TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371 | | | | U.S. APPLICATION NO. (If known, see 37 CFR 1.5) 10/089488 | |
| INTERNATIONAL APPLICATION NO. PCT/GB00/03709 | | INTERNATIONAL FILING DATE 27 September 2000 | | PRIORITY DATE CLAIMED 27 September 1999 | |
| TITLE OF INVENTION A RADIATION SOURCE | | | | | |
| APPLICANT(S) FOR DO/EO/US Donald Dominic ARNONE et al | | | | | |

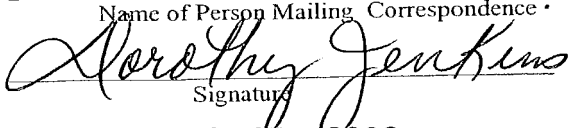
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

- ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
- ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
- ☒ This is an express request to promptly begin national examination procedures (35 U.S.C. 371(f)).
- ☒ The US has been elected by the expiration of 19 months from the priority date (PCT Article 31).
- ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2))
 - ☐ is attached hereto (required only if not communicated by the International Bureau).
 - ☒ has been communicated by the International Bureau.
 - ☐ is not required, as the application was filed in the United States Receiving Office (RO/US).
- ☐ An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)).
- ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3))
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 - ☐ have been communicated by the International Bureau.
 - ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - ☒ have not been made and will not be made.
- ☐ An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
- ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
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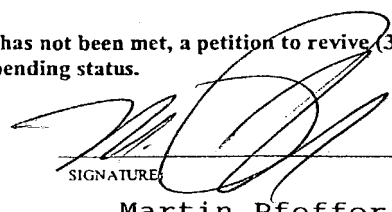
Items 11 to 16 below concern document(s) or information included:

- ☒ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
- ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
- ☒ A **FIRST** preliminary amendment.
☐ A **SECOND** or **SUBSEQUENT** preliminary amendment. EXPRESS MAIL CERTIFICATE
- ☐ A substitute specification.
- ☐ A change of power of attorney and/or address letter.
- ☒ Other items or information:
 Print EFS Form
 21 Drawing Sheets (Figs. 1-23)
 Intl. Search Report
 Intl. Prelim. Exam. Report

I hereby certify that this correspondence is being deposited with the United States Postal Service as Express Mail Post Office to Addresses (mail label
EL924372496US in an envelope addressed to:
 U.S. Patent and Trademark Office, P.O.
 Box 2327, Arlington, VA 22202 on
 March 27, 2002

Dorothy Jenkins
 Name of Person Mailing Correspondence

 Signature
 March 27, 2002
 Date of Signature

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| 17. <input checked="" type="checkbox"/> The following fees are submitted: BASIC NATIONAL FEE (37 CFR 1.492(a)(1)-(5)): Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO \$1,040.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO 890.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO 740.00 International preliminary examination fee paid to USPTO (37 CFR 1.482) but all claims did not satisfy provisions of PCT Article 33(1)-(4) 710.00 International preliminary examination fee paid to USPTO (37 CFR 1.482) and all claims satisfied provisions of PCT Article 33(1)-(4) \$100.00 ENTER APPROPRIATE BASIC FEE AMOUNT = | | | | CALCULATIONS PTO USE ONLY | | |
| | | | | | | |
| Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)). | | | | \$ | | |
| CLAIMS | NUMBER FILED | NUMBER EXTRA | RATE | | | |
| Total claims | 23 - 20 = | 3 | X \$18.00 | \$ | 54.00 | |
| Independent claims | 7 - 3 = | 4 | X 84.00 | \$ | 336.00 | |
| MULTIPLE DEPENDENT CLAIM(S) (if applicable) | | | + 280.00 | \$ | | |
| TOTAL OF ABOVE CALCULATIONS = | | | | \$ | 1,280.00 | |
| <input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2. | | | | \$ | | |
| SUBTOTAL = | | | | \$ | 1,280.00 | |
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| TOTAL NATIONAL FEE = | | | | \$ | 1,280.00 | |
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| TOTAL FEES ENCLOSED = | | | | \$ | 1,280.00 | |
| | | | | Amount to be refunded: | \$ | |
| | | | | charged: | \$ | |
| a. <input checked="" type="checkbox"/> A check in the amount of \$ <u>1,280.00</u> to cover the above fees is enclosed. Check No. 8887 | | | | | | |
| b. <input type="checkbox"/> Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees. A duplicate copy of this sheet is enclosed. | | | | | | |
| c. <input checked="" type="checkbox"/> The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. <u>15-0700</u> . A duplicate copy of this sheet is enclosed. | | | | | | |
| NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status. | | | | | | |
| SEND ALL CORRESPONDENCE TO: OSTROLENK, FABER, GERB & SOFFEN, LLP 1180 Avenue of the Americas New York, NY 10036-8403 Tel: (212) 382 0700 | | | | | | |
| | | | | SIGNATURE |  Martin Pfeffer NAME 20,808 REGISTRATION NUMBER | |
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JC05 Rec'd PCT/PTO 27 MAR 2002

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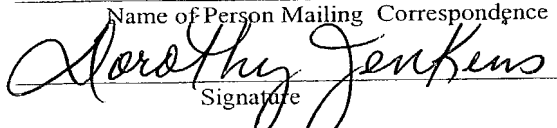
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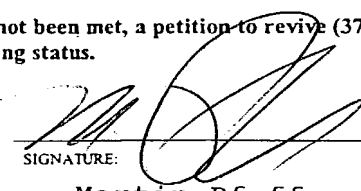
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(Figs. 1-23)
Intl. Search Report
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EXPRESS MAIL CERTIFICATE

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Box 2327, Arlington, VA 22202 on
March 27, 2002

Dorothy Jenkins
Name of Person Mailing Correspondence

Signature
March 27, 2002
Date of Signature

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| | | | | SIGNATURE:  Martin Pfeffer NAME 20,808 REGISTRATION NUMBER | |

P/25-277

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Patent Application of

Donald Dominic ARNONE et al

Date: March 27, 2002

Serial No.:

Group Art Unit:

Filed:

Examiner:

For: A RADIATION SOURCE

U.S. Patent and Trademark Office
P.O. Box 2327
Arlington, VA 22202

Attn: Box PCT (US/DO/EO)

AMENDMENT/SUBMISSION

Prior to examination, please amend the application as follows.

FEE CALCULATION

Any additional fee required has been calculated as follows:

_____ If checked, "Small Entity" status is claimed.

| | NO. CLAIMS AFTER AMENDMENT | | HIGHEST NO. PREVIOUSLY PAID FOR | | EXTRA PRESENT | | RATE | ADDIT. FEE |
|--|----------------------------------|-------|---------------------------------------|------|---------------|---|---------------------|---------------|
| TOTAL | 23 | MINUS | 20 | * = | 3 | X | (\$9 SE or \$18) | \$ 54.00 |
| INDEP. | 7 | MINUS | 3 | ** = | 4 | X | (\$42 SE or \$84) | \$ 336.00 |
| FIRST PRESENTATION OF MULTIPLE DEPENDENT CLAIM | | | | | | X | (\$140 SE or \$280) | \$ |

* not less than 20 ** not less than 3

TOTAL \$ 390.00

If any additional payment is required, a check which includes the calculated fee of
\$390.00 (OFGS Check No. 8887) is attached.

In the event the actual fee is greater than the payment submitted or is inadvertently not
enclosed or if any additional fee during the prosecution of this application is not paid, the Patent
Office is authorized to charge the underpayment to Deposit Account No. 15-0700.

CONTINGENT EXTENSION REQUEST

If this communication is filed after the shortened statutory time period had elapsed and no separate Petition is enclosed, the Commissioner of Patents and Trademarks is petitioned, under 37 C.F.R. § 1.136(a), to extend the time for filing a response to the outstanding Office Action by the number of months which will avoid abandonment under 37 C.F.R. § 1.135. The fee under 37 C.F.R. § 1.17 should be charged to our Deposit Account No. 15-0700.

AMENDMENTS

X If checked, amendment(s) to the specification and/or claims are submitted herewith.

1. Claims:

Please cancel claims 1-25 without prejudice.

Please add new claims 26-48 pursuant to 37 C.F.R. § 1.121(c)(i) as set forth in the “clean” version attached hereto as Appendix A. Entry is respectfully requested.

REMARKS/ARGUMENT

This Preliminary Amendment is being submitted to place the claims in better form for U.S. practice and to reduce the government filing fee.

EXPRESS MAIL CERTIFICATE

I hereby certify that this correspondence is being deposited with the United States Postal Service as Express Mail to Addressee (mail label # EL924372496US) in an envelope addressed to: U.S. Patent and Trademark Office, P.O. Box 2327, Arlington, VA 22202, on March 27, 2002:

Dorothy Jenkins

Name of Person Mailing Correspondence


Signature

March 27, 2002

Date of Signature

Respectfully submitted,



Martin Pfeffer

Registration No.: 20,808

OSTROLENK, FABER, GERB & SOFFEN, LLP

1180 Avenue of the Americas

New York, New York 10036-8403

Telephone: (212) 382-0700

APPENDIX A
“CLEAN” VERSION OF EACH PARAGRAPH/SECTION/CLAIM
37 C.F.R. § 1.121(b)(ii) AND (c)(i)

CLAIMS (with indication of amended or new):

(New) 26. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation, the source being subjected to a magnetic field wherein the free carrier concentration of the frequency conversion member and the applied magnetic field is configured such that the cyclotron diameter of the free carriers of the frequency conversion member is within 30% of their scattering length.

(New) 27. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam having a frequency different to that of the emitted beam of radiation, the source being subjected to a magnetic field, the magnetic field and fluence of the input beam being configured to minimize the screening effect of free carriers in the frequency conversion member.

(New) 28. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted beam, the frequency conversion member comprises a magnetic material dopant.

(New) 29. The radiation source of claim 28, wherein the dopant is Mn.

(New) 30. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to being irradiated with an input beam with a frequency different to that of the emitted beam, the source being subjected to a magnetic field, the source further comprising means for applying an electric field at the surface of the frequency conversion member which is irradiated by the input beam.

(New) 31. The radiation source of claim 30, wherein the means for applying an electric field comprise a pair of Ohmic contacts provided to the frequency conversion member and means for applying a potential difference across said Ohmic contacts.

(New) 32. The radiation source of claim 30, wherein the Ohmic contacts have a substantially triangular shape such that the contacts taper towards one another.

(New) 33. The radiation source of claim 30, wherein the means for applying a field comprises a Schottky gate provided on the surface of the frequency conversion member which is irradiated by the input beam.

(New) 34. The radiation source of claim 26, wherein the input beam is circularly or elliptically polarized.

(New) 35. The radiation source of claim 26, wherein the magnetic field has a component parallel to that of the emitted beam.

(New) 36. The radiation source of claim 26, wherein the emitted beam is produced by reflection of the input beam off a surface of the frequency conversion member.

(New) 37. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation, the source being subjected to a magnetic field which has a component parallel to that of the emitted beam of radiation, the emitted beam of radiation being produced by reflecting the input beam off a surface of the frequency conversion member.

(New) 38. The radiation source of claim 26, wherein the magnetic field is oriented parallel to the emitted beam.

(New) 39. The radiation source of claim 26, wherein the magnetic field is oriented at an angle of at most 20° to the emitted beam.

(New) 40. The radiation source of claim 26, wherein the frequency conversion member is selected from InAs, InSb and GaAs.

(New) 41. The radiation source of claim 26, configured such that the angle between the input beam and the surface normal of the frequency conversion member is substantially the Brewster angle.

(New) 42. The radiation source of claim 26, wherein the frequency conversion member is subjected to a magnetic field of at least 2T.

(New) 43. The radiation source of claim 26, the source further comprising a magnet to apply the said magnetic field.

(New) 44. The radiation source of claim 26, wherein the emitted radiation comprises at least one frequency in the ranges from 0.1 THz to 100THz.

(New) 45. The radiation source of claim 26, wherein the input beam is a pulsed beam.

(New) 46. a method of optimizing a radiation source, the radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation.

(New) 47. A method of optimizing a radiation source, the radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation,
the method comprising the step of applying a magnetic field to the source, the fluence of the input beam being chosen in order to minimize the screening of the surface field of the frequency conversion member by free carriers in the frequency conversion member for a predetermined magnitude of the applied magnetic field.

(New) 48. The method of claim 46, wherein the magnitude of the applied magnetic field or the optical fluence is determined by the steps of:

a) measuring the power of the emitted beam as a function of optical fluence for at least three values of magnetic field;

b) fitting the data measured in a) to the relation:

$$P \propto \frac{n^2 B^2}{m^4} x \left[\frac{\cos \theta_M \sin \theta_M}{2\theta_M} + \frac{1}{2} \right], \quad (1)$$

where P is the power of the emitted beam, n is the free carrier concentration, m is the effective mass of the carriers, B is the magnetic field and θ_M is:

$$\theta_M(n, B) = \arccos \left[1 - \frac{1}{2} \left(\frac{\lambda}{r} \right)^2 \right], \quad (2)$$

where λ is the mean free path which is defined as $\frac{1}{2}(n^{-1/3})$ and r is the cyclotron radius;

c) determining the fluence values for the at least three values of magnetic field where with increasing fluence the measured power starts to diverge from the function of step b); and

d) fitting an exponential function to the at least three values determined in point c) such that the optimum fluence can be determined for a given magnetic field or an optimum magnetic field can be determined for a given fluence.

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A Radiation Source

The present invention primarily relates to a radiation source for emitting radiation with frequencies ranging from the high Gigahertz range (GHz) up to and including the Terahertz range (THz). All such radiation is colloquially known as THz radiation, especially that in the range from 0.1 THz to 100 THz. More specifically, the present invention relates to a magnetically enhanced radiation source for such radiation.

Recently, there has been much interest in using THz radiation to look at a wide variety of samples using a range of methods. THz radiation has been used for both imaging samples and obtaining spectra. Recent work by Arnone et al, SPIE, European Conference Munich, June 1999, illustrates the use of THz radiation to image types of human and non human tissue.

THz radiation is of particular use because it penetrates most dry, non metallic and non polar objects like plastics, paper, cardboard and non polar organic substances. Therefore, THz radiation can be used instead of x-rays to look inside boxes, cases etc. THz has lower energy, non-ionising photons than X-rays, hence, the health risks of using THz radiation are expected to be vastly reduced compared to those using conventional X-rays.

To improve the usefulness of such THz radiation, there is a need to produce a THz source which can produce a relatively high energy beam of THz. To date, there are no compact solid state sources of THz radiation. However, recent advances in ultra fast pulsed lasers operating in the near infrared and visible have allowed coherent, broadband THz pulses to be produced from semiconductors. There are three widely-used methods for generating coherent THz from semiconductors irradiated by such ultrafast pulses : optical rectification, the surface field photocurrent effect, and lateral

photocurrent effect using antennas. THz radiation is produced by irradiating a semiconductor material which possesses suitable properties with an input beam of optical or infra-red radiation which can be produced by a standard laser such as a Ti:Sapphire Laser. It would seem logical that to produce a strong THz source, all is required is a stronger input beam. However, this is not the case as the power of the emitted THz beam saturates as the power of the input beam is increased. Also, higher input beam powers may damage the crystal being irradiated.

It has been previously suggested that the THz output of such a semiconductor material can be controlled by subjecting the material to a magnetic field. Zhang et al. Appl. Phys. Lett. 62 2003 (1993) showed that the direction and polarisation of a THz beam produced from a non-linear semiconductor crystal (in this case GaAs) could be controlled by subjecting the non-linear material to a magnetic field. The magnetic field here was oriented perpendicular to both the input beam and the THz beam. The THz beam was produced by transmission of the input beam through the non-linear material.

Some et al. Phys. Rev. B 53, R13 295 (1996) also used transmission geometry to investigate how THz emission using transmission geometry was affected by an applied magnetic field. Here, the field was applied both perpendicular to the input beam (and hence perpendicular to the emitted beam) and also at an angle of 25° from the input beam.

Sarukura et al. Appl. Phys. Lett. 84, 654 (1998) have recently shown enhanced THz emission using reflection geometry. Here, the non-linear material was positioned at 45° to the input beam, such that the emitted (or more correctly, the reflected) beam and input beam are arranged at right angles. In this arrangement, the magnetic field was arranged parallel to the input beam, but perpendicular to the emitted beam. Using a magnetic field with a strength of 1.7T, Sarukura et al. achieved a THz beam having a power of several μ watts with a 1.5 W excitation power.

The present invention addresses the above problem of providing an enhanced source which is intended primarily for use on the THz frequency range and which has obtained better results than the previously discussed methods for enhancing THz emission.

In a first aspect, the present invention provides a radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation, the source being subjected to a magnetic field which has a component parallel to that of the emitted beam of radiation, the emitted beam of radiation being produced by reflecting the input beam off a surface of the frequency conversion member.

The source is primarily intended for use in the THz frequency range. Preferably, the emitted radiation has a frequency in range of 0.1 THz to 100THz, more preferably from 1THz to 84THz even more preferably, from 1 THz to 20 THz.

Reflection geometry is chosen as there are losses in the radiation power as the THz beam transverses the frequency conversion member in transmission geometry.

The radiation source of the present invention is capable of producing a more efficient THz beam. The source of Sarukura et al. is capable of a conversion efficiency of 4.3×10^{-5} . However, the present invention is capable of a conversion efficiency in excess of this figure. For example, the present invention has obtained conversion efficiencies of 4.3×10^{-3} .

Preferably, the magnetic field is arranged at an angle of 20° or less to the emitted or reflected beam. More preferably, the magnetic field is arranged completely parallel to the emitted or reflected beam.

A number of different frequency conversion member could be used for example LiIO_3 , $\text{NH}_4\text{H}_2\text{PO}_4$, ADP, KH_2AsO_4 , Quartz, AlPO_4 , ZnO, CdS, GaP, GaAs, BaTiO_3 , LiTaO_3 ,

LiNbO₃, Te, Se, ZnTe, ZnSe, Ba₂NaNb₅O₁₅, AgAsS₃, proustite, Cd, Se, CdSe, CdGeAs₂, AgGaSe₂, AgSbS₃, ZnS, BBO, KTP, DAST (4-N-methylstilbazolium), L₄NbO₃. The frequency conversion member will preferably be one of InAs, InSb or GaAs.

The magnetic field may be generated by an electro-magnet or a permanent magnet. The source may comprise such a magnet. Preferably the frequency conversion member is cooled.

Experiments using sources according to the above mentioned aspects of the present invention have shown that the conversion efficiency does not saturate with magnetic field for an appropriate choice of incident pump energy per unit area (optical fluence). Therefore, preferably, the frequency conversion member is subjected to a magnetic field of at least 2T.

How the efficiency of the emitted beam varies with the applied magnetic field is believed to be determined by at least three principal effects, the acceleration of surface charge due to the Lorentz force in a magnetic field; the carrier-carrier scattering of the free carriers of the frequency conversion member and the screening of the surface field of the frequency conversion member. Acceleration of charge due to Lorentz force in magnetic field, given by the formula:

$$E_{rad} \propto dJ / dt \propto dv / dt \propto E_{surf} + v \times B \quad (0)$$

where E_{rad} is the field of the radiation, J is the surface current, v is the velocity of charged force carriers and E_{surf} is the surface field.

Maximising the acceleration of charge will in general maximise the power of the emitted beam. The application of a magnetic field enhances the acceleration. However, the acceleration can be further enhanced by using a frequency conversion member which has been magnetically doped.

It has previously been shown that a large Faraday effect can be seen in semiconductors which have been doped using magnetic ions such as Mn.

In a second aspect, the present invention provides a radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to being irradiated with an input beam with a frequency different to that of the emitted beam, the frequency conversion member being doped with a magnetic material.

In use, the source is subjected to a magnetic field.

More preferably, the magnetic dopant is Mn. However, other magnetic dopants such as Tc or Re could be used.

The acceleration can also be enhanced by applying an electric field to the frequency conversion member in addition to the magnetic field.

Therefore, in a third aspect, the present invention provides a radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to being irradiated with an input beam with a frequency different to that of the emitted beam, the source being subjected to a magnetic field, the source further comprising means for applying an electric field at the surface of the frequency conversion member which is irradiated by the input beam.

The means for applying the electric field can be provided by two Ohmic contacts provided to the frequency conversion member and means for applying a bias to accelerate the photocarriers between these two contacts. The Ohmic contacts may be shaped so that they taper towards one another. In other words, they form a "bow-tie" shape.

The means may also be provided by a front gate which overlies the surface of the frequency conversion member which is irradiated by the input beam.

Preferably, the frequency conversion member comprises a magnetic dopant. More preferably, the magnetic dopant comprises Mn. Also, the input beam is preferably circularly polarised.

In the radiation sources of the second and third aspect of the present invention, the magnetic field preferably has a component parallel to that of the emitted beam. More preferably, the magnetic field is at an angle of at most 20° to the emitted beam.

More preferably, the emitted beam is produced by reflection of the input beam off a surface of the frequency conversion member.

Although it is always desirable to enhance the acceleration of the charge, scattering and screening also affect the efficiency of the source. The source can be viewed as having a low optical fluence regime and a high optical fluence regime. In the low fluence regime carrier-carrier scattering is the dominant mechanism limiting the enhancement of the power of the emitted beam. In the high fluence regime, screening of the surface electric field is the dominant mechanism which limits the enhancement of the power of the emitted beam.

In the presence of a fixed magnetic field such as one might find in a superconducting magnet in persistent mode (the type found for example in MRI machines) or a fixed permanent magnet, the two optical fluence regimes can be determined by plotting out the experimentally measured power of the emitted beam as function of adjusted optical fluence (determined by laser power and/or spot size adjustment, or other means) for different magnetic field values.

The time-averaged power of the emitted beam can be approximated with the expression:

$$P \propto \frac{n^2 B^2}{m^4} \left[\frac{\cos \theta_M \sin \theta_M}{2\theta_M} + \frac{1}{2} \right], \quad (1)$$

where P is the power of the emitted beam, n is the free carrier concentration, m is the effective mass of the carriers, B is the magnetic field, and θ_M represent the angle completed by the carrier at the time of the collision, and r is the cyclotron radius. This angle can be expressed as a function of the ratio $R = \lambda/r$ of the characteristic radius as

$$\theta_M = \arccos \left[1 - \frac{1}{2} \left(\frac{\lambda}{r} \right)^2 \right], \quad (2)$$

where λ is the mean free path which is defined as $n^{-1/3}/2$.

The above expression is only valid for $(\lambda/r) < \sqrt{2}$. For magnetic fields B smaller than 10T, (2) can be approximated as a linear function of B , $\theta_M \approx \alpha B$. In this limit, (1) reduces to:

$$P \propto \frac{1}{m^*} \left[\frac{B \sin(2\alpha B)}{4\alpha} + \frac{B^2}{2} \right] \quad (3)$$

Fitting the calculated emitted beam power of (1) as function of optical fluence (or equivalently, photogenerated carrier density n) with the measured values allows one to determine whether one is in the low or high optical fluence limit.

In the low fluence limit it is possible to fit (1) to the experimental data by applying a suitable multiplicative factor to one or the other data set. In the high fluence limit, there is significant deviation of experimental data below the prediction of (1) as the optical fluence increases.

In this high fluence regime, it is believed that screening dominates and reduces the source efficiency, i.e. the (emitted beam power)/(the input beam power) as the optical fluence increases. In the high optical fluence regime, screening of the surface field becomes the dominant mechanism, and the term E_{surf} is dramatically reduced.

It is often desirable to generate the largest power possible from a source. Increasing the power of the input beam will in most (but not all) cases increase the power of the emitted beam. However, the screening which occurs in the high fluence regime means that once the high fluence regime is entered, the efficiency of the source decreases. Hence, it is not desirable to increase the input beam power to enter this regime. Therefore, there is a need to be able to determine the start of this regime. The inventors of the present invention have determined how to establish this and have also surprisingly found that the point at which this regime is entered is dependent upon the applied magnetic field as well as the fluence of the input beam.

Therefore, according to a fourth aspect, the present invention provides a radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam having a frequency different to that of the emitted beam of radiation, the source being subjected to a magnetic field, the magnetic field and fluence of the input beam being configured to minimise the screening effect of free carriers in the frequency conversion member.

In fifth aspect, the present invention provides a method of optimising a radiation source, the radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation,

the method comprising the step of applying a magnetic field to the source, the magnitude of the magnetic field being chosen in order to minimise the screening of the surface field of the frequency conversion member by free carriers in the frequency conversion member for a predetermined fluence of the input beam.

In a sixth aspect, the present invention provides a method of optimising a radiation source, the radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation,

the method comprising the step of applying a magnetic field to the source, the fluence of the input beam being chosen in order to minimise the screening of the surface field of the frequency conversion member by free carriers in the frequency conversion member for a predetermined magnitude of the applied magnetic field.

In the high optical fluence regime, the efficiency of the source can be optimised by determining the point at which the measured power deviates from the predicted value of (1) with increasing optical fluence for the applied magnetic field. It has been found that the point at which the emitted power deviates from that predicted by (1) varies exponentially with applied magnetic field. Therefore, by measuring the divergent values, it is possible to predict the optimum optical fluence for a given magnetic field and vice versa.

Therefore, preferably, the method of the fifth and sixth aspects of the present invention determine the magnitude of the magnetic field or the optical fluence by the steps of:

- a) measuring the power of the emitted beam as a function of optical fluence for at least three values of magnetic field;
- b) fitting the data measured in a) to the relation:

$$P \propto \frac{n^2 B^2}{m^4} \left[\frac{\cos \theta_M \sin \theta_M}{2\theta_M} + \frac{1}{2} \right], \quad (1)$$

where P is the power of the emitted beam, n is the free carrier concentration, m is the effective mass of the carriers, B is the magnetic field and θ_M is :

$$\theta_M(n, B) = \arccos \left[1 - \frac{1}{2} \left(\frac{\lambda}{r} \right)^2 \right], \quad (2)$$

where λ is the mean free path which is defined as $1/2(n^{-1/3})$ and r is the cyclotron radius;

c) determining the fluence values for the at least three values of magnetic field where with increasing fluence, the measured power starts to diverge from the function of step b); and

d) fitting an exponential function to the at least three values determined in point c) such that the optimum fluence can be determined for a given magnetic field or an optimum magnetic field can be determined for a given fluence.

Preferably, the fitting in step (b) is performed by weighting the points with a lower optical fluence.

The exponential fit in step (d) is preferably made to the function having the general form:

$$F=F_0+A\exp(B/t)$$

where F is the fluence, B the magnetic field and F_0 , A and t are the parameters to be fitted. Once these parameters are determined, the optimum fluence for a given magnetic field or the optimum field for a given fluence can be determined.

The fluence values where the measured power starts to diverge can be taken as where the measured power drops more than 10% below the theoretical value, more preferably more than 5% below the theoretical value.

In the limit of low fluence, electron-electron scattering will reduce THz power appreciably until the limit where the cyclotron diameter (2r) is comparable to the electron-electron scattering length, i.e. 2r is close to the electron-electron scattering length $\lambda=n^{-1/3}/2$.

Therefore, in a seventh aspect, the present invention provides a radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation response to irradiation with an input beam with a frequency different to that of

the emitted radiation, the source being subjected to a magnetic field wherein the free carrier concentration of the frequency conversion member and the applied magnetic field is configured such that the cyclotron diameter of the free carriers in the frequency conversion member is within 30% of their scattering length.

The scattering length being defined by $\lambda = n^{-1/3}/2$. The cyclotron diameter can be 30% larger or 30% smaller than the scattering length.

Preferably, the cyclotron diameter of the free carriers is within 20% of the carrier-carrier scattering length, more preferably 10%, even more preferably 5%.

Both the cyclotron diameter and the electron-electron scattering length are dependent on B and n (optical fluence). Thus, these need to be optimised simultaneously.

Scattering between adjacent electrons results in decoherence of the waveforms of the emitted beam and hence reduce the emitted power. Decoherence here means that the emitted waveforms from the accelerated charge do not add or combine constructively, i.e. no constructive interference. In general, electron-electron (or more generally carrier-carrier) scattering is the dominant mechanism at lower optical fluences, leading to low photogenerated carrier densities. The above ensures that the length of the electron trajectory s is maximised before scattering off the next adjacent electron located λ away.

Typically, the wavelength of the input or pump beam for any of the above sources will be such that the photon pump energy is larger than the band gap of the frequency conversion member. Preferably, source will be configured such that the input beam is at the Brewster angle of the frequency conversion member, i.e. at the Brewster angle to the surface normal. The Brewster angle will be about 70° to the surface normal. Therefore, typically, the input beam will be preferably arranged between 45° and 85°, more preferably between 60° and 80°.

It should be noted that a radiation source may be provided which comprises any combination of a magnetically doped frequency conversion member and means for applying an electric field to the frequency conversion member. This source may also be configured with the reflection geometry of the first aspect of the present invention. The applied magnetic field and the fluence of the input beam may also be optimised to reduce scattering or screening effects in a source having a magnetically doped frequency conversion member and/or means for applying an electric field to the frequency conversion member and/or which is configured with the reflection geometry of the first aspect of the present invention.

All of the above sources are preferably used to generate radiation having at least one frequency in the range from 0.1 THz to 100 THz. The input beam may be a pulsed beam or a so-called CW beam.

The present invention will now be described with reference to the following preferable, non-limiting embodiments, in which:

Figure 1 is a schematic of a source in accordance with an embodiment of the present invention;

Figure 2 is a schematic of the experimental arrangement to measure a source according to an embodiment of the present invention;

Figures 3a and 3b are plots of the transverse magnetic and transverse electric polarisation direction of a THz electric field emitted by a source according to an embodiment of the present invention;

Figure 4 shows a plot of the transverse magnetic polarisation component of a THz emission spectra from a source according to an embodiment of the present invention;

Figures 5a and 5b show plots of the power calculated from the transverse magnetic and the transverse electric polarisations respectively, figure 5c plots the total power;

Figure 6 is a plot of THz power from an InAs source according to an embodiment of the present invention;

Figure 7 shows a plot of THz conversion efficiency and THz pulse energy against the energy of the visible pulse;

Figure 8 is a plot comparing the efficiency of THz generation according to an embodiment of the present invention as compared with the known prior art;

Figure 9 shows a compact THz emitter in accordance with an embodiment of the present invention;

Figure 10 shows a compact THz emitter in accordance with a further embodiment of the present invention;

Figure 11 shows a compact emitter in accordance with another embodiment of the present invention;

Figure 12 shows a THz emitter in accordance with another embodiment of the present invention;

Figure 13 shows a variation on the emitter of Figure 12;

Figure 14 shows a magnetically doped THz emitter in accordance with an embodiment of the present invention;

Figure 15 shows an experimental arrangement for detecting THz radiation from the source of Figure 14;

Figure 16 shows an embodiment of the present invention which uses an electric field as well as a magnetic field to enhance THz production;

Figure radiation with at least one frequency in the range from 0.1 THz to 100 THz 17 shows a further embodiment of the present invention where a front gate overlies a surface of the THz emitter;

Figure 18 shows a plot of the power of the emitted beam against the optical fluence of the input beam for a source in accordance with an embodiment of the present invention;

Figure 19 shows a schematic cyclotron orbit of a carrier in the frequency conversion member of a source in accordance with an embodiment of the present invention;

Figure 20 shows a plot of the cyclotron orbit radius against the optical fluence of the input beam of a source in accordance with an embodiment of the present invention;

Figure 21 shows a plot of the power of the emitted THz beam against the applied magnetic field of a source in accordance with an embodiment of the present invention;

Figure 22 shows a Monte Carlo simulation of the electric field against depth from the surface of a source in accordance with an embodiment of the present invention; and

Figure 23 shows a plot of optical fluence of the input beam against the applied magnetic field for a source in accordance with an embodiment of the present invention, the solid line shows the optimal magnetic field for a set fluence.

Figure 1 shows a THz emitter according to an embodiment of the present invention. The THz emitter has a frequency conversion member 1 which is either InAs, InSb, or GaAs.

It should be noted that other types of frequency conversion member are possible either crystalline or non-crystalline. For example, LiIO_3 , $\text{NH}_4\text{H}_2\text{PO}_4$, ADP, KH_2AsO_4 , Quartz, AlPO_4 , ZnO , CdS , GaP , GaAs , BaTiO_3 , LiTaO_3 , LiNbO_3 , Te , Se , ZnTe , ZnSe , $\text{Ba}_2\text{NaNb}_5\text{O}_{15}$, AgAsS_3 , proustite, Cd , Se , CdSe , CdGeAs_2 , AgGaSe_2 , AgSbS_3 , ZnS , BBO , KTP , DAST (4-N-methylstilbazolium), LiNbO_3 .

A pump beam 3 is directed towards member 1 at an angle θ_i to the surface normal of member 1. The pump beam is reflected from the surface 5 of emitter 1 as a THz beam at an angle θ_r to the surface 5 normal. The emitter is subject to a magnetic field along the direction of the emitted THz beam 7. As the magnetic field direction 9 is parallel to the direction of the THz beam 7, both the transverse electric $P_{\text{THz}}T_E$ and the transverse magnetic $P_{\text{THz}}T_M$ polarisation components of the THz beam are subject to a magnetic field.

The pump beam will typically have wavelengths in the range 2mm to 350nm. The pump wavelength will be such that the pump photon energy is larger than the band gap energy of the frequency conversion member 1. The pump beam will be a pulsed beam with a plurality of frequencies contained within each pulse. The semiconductor frequency conversion member 1 can emit a THz beam that is a difference of two of the frequencies in the pump beam.

Figure 2 shows an experimental arrangement which is used to generate THz in accordance with an embodiment of the present invention. A mode-locked Ti:Sapphire Laser 21 produces a beam 23 of 90 fs pulses at a wavelength of 790nm and a repetition rate of 82MHz. Beam 23 yields 0.8W average power and has pulse energies in the nJ range. Beam 23 is split by beamsplitter 25 into a pump beam 27 and a probe beam 29. Eventually, it will be required to bring the probe beam and the pump beam back into synchronisation with one another or change the temporal shift between the pump beam and the probe beam. Therefore, the pump beam 27 is reflected off mirror 31. Thus, the path length of pump beam 27 can be varied. Mirror 31 reflects pump beam 27 through half wave plate 33 and into polariser 35. The polariser 35 transmits the beam onto

mirror 37 which then reflects the beam through lens 39 and cryostat windows (e.g. Spectrosil B) 41 and 43 onto crystal 45. After the beam has passed through chopper 38, the beam is transmitted through lens 39. Crystal 45 is a frequency conversion member and is situated in a magnetic field. Emitter crystal 45 is also angled at 45° to the incident pump beam 27. Chopper 38 functions to chop the beam at a certain frequency. This can improve detection as the beam can be detected at the chopper 38 frequency using a lock-in amplifier. For this type of system, the chopper 38 will preferably be an acousto-optic modulator. Angles of Brewster's angle for the crystal source in question are preferable. For InAs, InSb and GaAs, the Brewster angle is about 70°. Thus, a reflected THz beam 47 is reflected from crystal 45 at an angle of 90° to pump beam 27. The magnetic field generated by a split coil superconducting magnet 49 is parallel to the direction of the emitted THz beam 47. The emitted THz beam 47 is then passed through cryostat window 53 and THz polariser 55.

Figure 2 shows two methods for detecting the THz. The first of these is bolometer 57. This is a He-cooled bolometer which is placed immediately after the cryostat to allow efficient collection of the emitted THz. Bolometer 57 measures both coherent and incoherent contributions to the THz power. In both detection mechanisms, polariser 55 allowed selection of either the transverse electric or transverse magnetic THz polarisation with a 10% transmission loss. Losses by other elements in the THz beam path were determined using an infra red transform spectrometer and accounted for 50% loss at a frequency of 1 THz. The visible pump beam was also attenuated by 19% due to cryostat windows.

Either instead of or in addition to the bolometer, an electro-optic sampling detection mechanism 59 is also present in the apparatus of Figure 2.

The electric-optic sampling system 59 relies on the ac Pockels effect. The THz beam 47 is combined with pump beam 29 using mirror 61. Before passing through the back of mirror 61, probe beam 29 is passed through a polariser 63. The combined THz beam 47 and probe beam 29 are then directed onto a 1mm thick (110) ZnTe crystal. Due to the

ac pockels effect, the presence of THz beam 47 causes a rotation in the polarisation of pump beam 29. Therefore, the presence of THz can be detected. When the combined beam 63 has passed through detection crystal 65, it is then transmitted through quarter wave plate 65 to a Wollaston Prism 67 (or other polarisation splitting device) onto balanced photodiode arrangement 69.

If the polarisation of probe beam 29 has not been rotated, the balanced photodiode assembly will read 0. However, if the polarisation of the probe beam 29 has been rotated, there will be a difference in the intensity of the beams split by the Wollaston Prism which are detected by two photodiodes within the balance photodiode assembly 69. The difference in the output of the photodiodes will cause the magnitude of the output of the balance photodiode assembly to be greater than 0. The amount by which the polarisation of the probe beam 29 is rotated by the THz beam 47 is dependent on the intensity of the THz beam 47. Therefore, the output of the balance photodiode assembly 69 directly measures the electric field of the THz beam.

The evolution of the field with time is measured by varying the delay (via mirror 31) between the visible pump 27 and probe beams 29. The power spectrum associated with the THz radiation may be obtained by Fourier transforming the time-domain data. The bandwidth of the THz pulse measured using the electro-optic sampling detector 59 of Figure 2 extends from 0.5 THz to 2.7 THz. This bandwidth is in part constrained by the thickness of the detector crystal and prevents highly accurate measurement of enhancement at frequencies outside this range.

Figure 3a shows the variation in the intensity of the THz signal as the time delay between the probe beam and the pulse beam is varied using mirror 31 for magnetic fields from 0T-8T. Figure 3a shows the results for transverse magnetic polarisation and Figure 3b shows the results of transverse electric polarisation.

Figure 4 shows the THz power measured using the experimental set up of Figure 2 as a function of frequency obtained by Fourier transforming time-domain spectrum of the

type shown in Figures 3a and 3b. An enhancement occurs across the most accessible THz bandwidth, accompanied by a relatively large increase of the power at frequencies above 2.7 THz. The behaviour was also observed for the transverse electric polarisation and was reproduced in spite of the reduced accuracy of detection in this range.

The amount of coherent power can be determined from the area under the frequency of the main power spectrum between 0.5 and 2.7 THz. Calculating this power for both polarisation components, ie. transverse magnetic and transverse electric allows a direct comparison with magnetic field dependence of the bolometer measurements which are shown in Figure 5.

The dependence of the THz power on magnetic field is similar with the electro-optic sampling detector 59 and the bolometer 57 suggesting that the majority of field enhanced emission is coherent. There is a decrease in the intensity of the transverse magnetic polarisation component $B > 6T$ which is not present in the bolometer measurement. This suggests that there may be a peak in the enhancement of a coherently generated THz for this polarisation. Such a peak is not observed in the transverse electric polarisation. These results suggest a further increase in magnetic field B would yield in a larger enhancement of the coherently generated THz power.

Figure 6 shows the dependence of the bolometer power on magnetic field for both of the individual polarisation components (i.e. transverse electric and transverse magnetic) as well as the total value. It can be seen that if the magnetic field is increased, both polarisation components are also increased. The total power is 486mW at 8T after accounting for losses in both the cryostat and the polariser. Path lengths between the cryostats outer window and the bolometer were kept less than 5cm to minimise atmospheric absorption of the THz. Therefore, with an average incident pump power at the sample of 113mW, the average power visible to average THz power conversion efficiency is 0.43%.

These results clearly suggest that going to even higher magnetic fields will result in even higher THz efficiency.

Figure 7 shows results taken at 8T and 180K for (100)InAs as a generator crystal. Sample geometry is the same as that described with reference to Figures 1 and 2.

The x-axis shows the variation in the visible pulse energy of the pump beam. The left-hand y-axis shows the visible THz conversion efficiency and the right-hand y-axis shows the measured THz pulse energy. The open symbols shows the energy for an unamplified, conventional oscillator source, and the closed symbols show those for an amplifier system. The lines through the closed symbols and the open symbols relate to a double exponential fit to the results. This graph suggests that increasing the visible pulse energy does not necessarily provide an increase THz signal. Therefore, other methods of increasing the THz signal are of commercial significance.

Figures 8a and 8b compare results taken in accordance with an embodiment of the present invention. With those of the known prior art. Specifically, the data points A to J are as follows:

- A. 1mm (110) ZnTe at room temperature, with no magnetic field. Pumped with 100mW from an oscillator.
- B. (100) InAs at 173K and B=8T, applied parallel to the direction of the THz beam. Pumped 130mW average power from an oscillator in accordance with an embodiment of the present invention.

- C. (100) InAs at 173K and B=8T, applied parallel to the direction of the THz beam.

Pumped 83mW average power (0.33μJ pulse energy) from an amplifier in accordance with an embodiment of the present invention.

- D. (100) InAs at room temperature and $B=1.7T$, applied perpendicular to the direction of the THz beam. Pumped with 1.5W from an oscillator. (Sakura et al, J. App. Phys. 84 654).
- E. Large aperture photoconductive antenna on SI GaAs at room temperature, no magnetic field. Pumped with 882mW (4.4 μ J) from an amplifier. (Mouret et al Microwave Opt. Tech. Lett. 17 23).
- F. Large aperture photoconductive antenna on SI GaAs at room temperature, no magnetic field. Pumped with 500mW (500 μ J) from an amplifier. (Budiarto et al IEEE J. Quant. Elec. 32 1839).
- G. Large aperture photo conductive antenna on SI GaAs at room temperature, no magnetic field. Pumped with 2.8mW (282 μ J) from an amplifier. (You et al Opt. Lett. 18 290).

Figure 9 shows a compact emitter in accordance with an embodiment to the present invention. The emitter comprises an electro magnet or a permanent magnet 71 which has a hole 73 formed therethrough. Hole 73 completely penetrates the magnet 71 and defines a space for the THz emitter space. The space is boarded on four sides by magnet 71 and at the upper 78 and lower 77 surfaces by non-magnetic material. The visible pump beam 75 enters the lower surface 77 of the emitter space 73. The pump beam 75 enters the emitter through pump window 79. The pump beam 75 is reflected off mirror 81 onto emitter crystal 83. The emitter crystal is angled with respect to the magnet and the incident beam 75 so that the emitted THz 85 is parallel to the direction of the magnetic field. The THz 85 is transmitted through THz window 87 which is located in the upper surface 78 of emitter space 73.

Figure 10 shows a variation on the emitter of Figure 9. The same reference numerals are used to denote the same features in both Figures 9 and 10. Therefore, these features will not be repeated here. The compact emitter here is capable of being cooled to very

low temperatures. To achieve this cooling, the crystal 83 is mounted on a Peltier cooling element 89. The emitter space 73 has a vacuum port 91 such that the air within the emitter space can be evacuated.

Figure 11 shows a further variation on the compact emitter structure of Figures 9 and 10. Again, the description of like features will not be repeated. The detection crystal 83 is mounted on an electro magnet or a permanent magnet 93. The electro magnet or permanent magnet causes a magnetic field which is normal to the surface of the emitter crystal 83. The THz beam 85 is again produced by refraction of the pump beam 75 of the surface of the semiconductor emitter crystal 83. The angle of incidence of the pump beam 75 is chosen so that there will be a component of the magnetic field in the direction of the THz beam output 85.

The geometry in these and other figures is also chosen such that the angle of incidence of the pump beam qB is Brewster's angle for the crystal in question.

Figure 12 shows a further variation on the compact emitter structure. As for Figure 9, an electro magnet or permanent magnet 71 is formed with an aperture 73 which provides a sample space. The aperture is bounded at a lower surface 72 and an upper surface 74 by material which is not part of the magnet 71. A THz window 87 is formed in the upper surface of the bounding material 74. A hole 95 is formed in a side wall of the magnet 73. This hole forms a channel for the visible pump beam 75. The hole is positioned such that the visible pump beam can be shone through the hole directly onto emitter crystal 83 without the need of mirrors within the compact emitter itself. The reflected THz beam 85 is transmitted from the compact emitter through THz window 87.

Figure 13 shows a further variation on the emitter of Figure 12. Here, as described with reference to Figure 10, the crystal 83 is mounted on Peltier cooling element 89. The emitter space defined by aperture 73 must be evacuated. Therefore a vacuum port 91 is provided on a lower surface 77 of the compact emitter. The visible pump beam is again

introduced into the compact emitter along channel 95. The pump beam entering the emitter is sealed with a window or lens 97.

Figure 14 shows a THz emitter in accordance with a further embodiment of the present invention. The relationship between the input beam and the output beam with respective surface normal of the same as described with references to Figure 1.

Therefore, these features will not be repeated. However, the THz emitter crystal is different in Figure 14 to that of Figure 1. In Figure 14, the THz emitter crystal (101) is imbedded with magnetic ions Mn^{2+} . The strong S-D exchange interaction between the electron spins and the imbedded Mn^{2+} ions is known to amplify the frequency of the electron spin precession under the applied magnetic field. This results in field tuneable oscillations in the magnetic component of spin. It is known that these oscillations occur at THz frequencies. The frequencies given by the spin split energy $g\mu B$ where B is the applied magnetic field and μB is the Bohr magneton. The increase in energy owing to the presence of interactions between carriers and the magnetic ions is given by the enhanced value of the g factor, which ranges from 2 in non-magnetic samples all the way to 430 or larger in magnetic samples. It is believed that enhanced g -factors may result in accelerations associated with electron spin of the radiated $g\mu B$ in the THz range. In Figure 14, the magnetic field is arranged perpendicular to the surface normal and photo injected carrier spins.

Another mechanism for enhanced Terahertz emission from magnetically doped semiconductors is the enhanced internal magnetic field associated with the ions, which leads to further acceleration of charge in the semiconductor and hence higher Terahertz emission powers. With the application of a small external magnetic field (e.g. several hundred millitesla, readily achieved with permanent magnets), the moments of the Mn^{2+} ions are aligned.

One motivation for introducing magnetic ions into the semiconductor is to reduce the magnetic fields required for THz enhancement from the several Tesla values suggested above, which may require superconducting magnets, to $B < 2T$ achievable with

permanent or electromagnets. Moreover, even in semiconductors where significant enhancement of the visible to THz conversion efficiency occurs at low magnetic fields, the addition of magnetic ions will further enhance the field, and hence conversion efficiency, achievable. To see this, note the net field inside a magnetically-doped semiconductor is given by

$$B_{\text{net}} = B_{\text{applied}} + \mu_0 M_{\text{Mn}}$$

where B_{applied} is the externally applied field inside the semiconductor (denoted simply by B in the preceding discussion). μ_0 is the permeability and M_{Mn} is magnetization associated with the ions; thus $B_{\text{ion}} = \mu_0 M_{\text{Mn}}$ is the magnetic field in the semiconductor in the presence of the magnetic ions.

The ultrafast laser sources can be those described. The laser must operate at frequencies at or above the band gap of the material in order to create photocarriers. Circular polarisation of the pump beam is generally required, achieved using standard quarter wave plates, if the spin of the photocarriers is to be oriented parallel to the surface normal.

The magnetically doped may be fabricated in a number of ways:

Numerous types of magnetically doped frequency conversion members 101 are possible. Bulk $\text{Zn}_{1-x}\text{Mn}_x\text{Se}$ grown on $\langle 100 \rangle$ GaAs or other compatible substrates are one class of structure. $x=0$ to 0.1 have been studied using optical and ESR characterization techniques, but higher concentrations x are possible using MBE.

(Ga,Mn)As bulk layers are other systems for realising internal magnetic fields to supplement the externally applied field. (Ga,Mn)As can be grown on (001) GaAs substrates using techniques such as low temperature MBE. For example, 100nm GaAs buffer layers may be grown at 570 C, followed by 0.2mm $(\text{Al}_x\text{Ga}_{1-x})\text{As}_{0.8}$ etch stop layer for any processing and mesa isolation. This layer is grown at 670 C. Finally, a

2mm (Ga,Mn)As layer is grown. Typical Mn concentrations are in the range 0.043, although other concentrations are possible using MBE.

ZnCdSe/ZnSe quantum wells on <100> GaAs having different concentrations of Mn²⁺ form an important class of structures. Discrete fractional monolayer planes of the binary magnetic semiconductor MnSe are incorporated into the ZnCdSe wells. The quantum well region thus consists of monolayers of the randomly diluted quaternary alloy (ZnCd,Mn)Se separated by nonmagnetic layers of say Zn_{0.8}Cd_{0.2}Se. The introduction of magnetic ions into the crystal lattice greatly enhances the effective g factors of the electron and hole bands through strong spin sensitive J_{sp-d} exchange interaction between the s-like (p-like) conduction (valence) band and the local 3d electrons that comprise the spin-5/2 paramagnetic Mn²⁺ moment. There are advantages to various distributions of the magnetic ion layers in the quantum wells. For example, for a fixed number of Mn spins, the g-factor may be enhanced by spreading the distribution of MnSe from a single, thick layer placed at one position in the ZnCdSe well, to several layers distributed in different planes throughout the well. This also mitigated against dephasing phenomena due to ion-ion interactions.

Figure 15 shows an experimental arrangement for measuring THz output from a magnetically doped semi-conductor. As many of the features are the same as described in reference to Figure 2, these will not be repeated. The main variation on the equipment of Figure 2 is the variation in the orientation between the magnetic field and the emitted THz. Here, the pump beam is transmitted onto a magnetically doped semi-conductor crystal emitter in the direction parallel to the surface normal of the semi-conductor crystal emitter. The magnetic field B is arranged so that it is parallel to the surface of the semi-conductor crystal emitter. The THz beam (57) is emitted parallel to the surface normal of the emitter. The beam (47) is then reflected off beam-splitter (121) which reflects the THz-beam onto mirror (123) and into the electro-optic sampling unit (59). The beam-splitter (121) allows transmission of the pump beam onto the cryostat window. The beam splitter may be a suitable material such as cellulose nitrate,

mylar, or other materials that are ideally non-lossy and non-dispersive at both THz and visible/near-infrared frequencies.

Figure 16 shows a further embodiment of the present invention. Here, an external bias is applied via contacts 201) and 203 across the surface of the THz emission crystal 205. The THz emission crystal 205 can be any of the type previously described. It may also be a magnetically doped structure.

The incident pump beam 207 then impinges on the emitter 2 or 5 in the region between the two contacts 201 and 203. The bias between the two contacts causes a lateral photocurrent to arise. The magnetic field 209 is incident on the sample at an angle of θ (theta) so that the emitted THz experiences a component of the magnetic field. The THz may be emitted via refraction or transmission through the sample 205.

Contacts 201 and 203 may take many forms. For example, as shown is Figure 16a, the contacts may be regular, rectangular contacts. However, as shown in Figure 16b, the contacts may be made in the shape of a bow tie antenna.

The contacts 201 and 203 may be Ohmic contacts. The distance between the two contacts may be varied between several microns to several millimetres.

Figure 17 shows a further arrangement used to enhance the field at the surface to enhance THz emission. Figure 17a shows an experimental arrangement similar to that of Figure 1. However, here, the emitter crystal has a front gate 301 located on the surface on which the pump beam impinges. The front gate 301 is a Schottky gate, the gate acts to modify the shape of the surface field in the semiconductor to enhance the THz emission. The gradient to the surface field enhances carrier acceleration at the surface and this enhances THz emission.

Typically, the gate will be fabricated from Au, NiCr etc.

The previous embodiments have mainly concentrated on enhancing the THz output by increasing the acceleration of the charged carriers in the frequency conversion member by using techniques such as applying an electric field to the surface of the frequency conversion member, using magnetic dopants etc.

However, it is possible to also enhance the THz emission by careful choosing of the applied magnetic field and the free carrier concentration which is controlled by the optical fluence of the input beam.

Figure 18 shows a measurement from a source which comprises a undoped GaAs frequency conversion member, the incident radiation surface is (100), the optical fluence is varied from 50 to 900nJ/cm². The plot of Figure 18 is a logarithmic plot in both the x and y directions (Fluence of input beam and Power of emitted beam respectively).

The data is shown for four values of magnetic field: 2T (empty circles); 4T (solid circles); 6T (triangles) and 8T (squares). The 4T data has been fitted (as will be explained below) and is shown by the solid line. The plot demonstrates the cross over between the low fluence regime (where the data fits to the solid line) and the high fluence regime (where the data diverges below the solid line).

The scattering length of the free carriers in the frequency conversion member increases with applied magnetic field due to charge executing a larger portion of cyclotron orbit before scattering off in adjacent electron or other particles. Cyclotron orbits are given by the well known classical formula in one, two or three dimensions and depend on both the optically induced (pump-induced) carrier density n as well as the applied magnetic field B and the material dependent effective mass of the accelerated charge m .

Figure 18 shows the cross over from the low optical fluence limit to the high optical fluence regime. In the low regime, carrier-carrier scattering is the dominant mechanism which limits the enhancement of THz power and one set of design procedures is used.

In the high fluence limit, the screening of the electric field is the dominant mechanism limiting the enhancement of THz power.

In the presence of a fixed magnetic field such as one might find in a superconducting magnet in persistent mode (the type found for example in MRI machines) or a fixed permanent magnet, one of the best ways to determine the limit of the optical fluence is to plot out the experimentally measured THz power as function of adjusted optical fluence (determined by laser power and/or spot size adjustment, or other means). Along with this, one plots the relation which governs emitted power in the presence of carrier-carrier scattering. The time-averaged emitted power can be approximated with the expression:

$$P \propto \frac{n^2 B^2}{m^4} \left[\frac{\cos \theta_M \sin \theta_M}{2\theta_M} + \frac{1}{2} \right], \quad (1)$$

where P is the power of the emitted beam, n is the free carrier concentration, m is the effective mass of the carriers, B is the magnetic field and θ_M represents the angle completed by the carrier at the time of the collision, and r is the cyclotron radius. This angle can be expressed as a function of the ratio $R = \lambda/r$ of the characteristic radius as

$$\theta_M = \arccos \left[1 - \frac{1}{2} \left(\frac{\lambda}{r} \right)^2 \right], \quad (2)$$

which is only valid for $(\lambda/r) < \sqrt{2}$. For magnetic fields B smaller than 10T, (2) can be approximated as a linear function of B, $\theta_M \approx \alpha B$. In this limit, (1) reduces to

$$P \propto \frac{1}{m^4} \times \left[\frac{B \sin(2\alpha B)}{4\alpha} + \frac{B^2}{2} \right] \quad (3)$$

Comparing the Terahertz power P (1) as function of optical fluence (or equivalently, photogenerated carrier density n in (1)) with the experimental determination noted above allows one to determine whether one is in the low or high optical fluence limit.

In the low fluence limit the experimental data can be made to lie along the same line as that derived from (1) with a suitable multiplicative factor applied to one or the other data set. In the high fluence limit, there is significant deviation of experimental data below the prediction of (1) at higher optical fluences, whereas at lower fluences the lines coincide.

Put more succinctly, to determine the fluence limit, one first measures experimentally determined powers as a function of fluence and then fits them to (1), with weight given to the points at low fluence.

Figure 18 shows such a fit for $B=4T$. The fluence value at which divergence (expt data falls below predictions of (1)) between (1) and the experimental data occurs marks the boundary; fluences below this are in the low fluence limit, and fluences above it are in the high fluence limit.

In Figure 18, this occurs near fluences of 400 nJ/cm^2 for $B=4T$ in the case of GaAs. Figure 18 also demonstrates how the limit will vary with the value of B applied. The limit in which the system falls will be determined by the magnetic fields B provided by available magnets, and range of laser fluences available with the ultrafast laser. Choice of material system and its characteristics will also play a role.

Scattering is believed to be the main mechanism which is responsible for controlling the emitted THz power. Practical limits are also imposed by the availability of fields using permanent magnets and the high cost associated with superconducting magnets, which rises with magnetic field. The electron-electron scattering will reduce THz power appreciably until the limit where the cyclotron diameter is comparable to the electron-electron scattering length, i.e. $2r$ is preferably equal to, but may be less than the electron-electron scattering length $\lambda=n^{-1/3}/2$.

As both the cyclotron diameter and the electron-electron scattering length are dependent on B and n (optical fluence), these need to be optimised simultaneously. The design rule

therefore is to choose a magnetic field for a given fluence (or fluence for given magnetic field) such that $2r \sim \lambda$. Scattering between adjacent electrons result in decoherence of the Terahertz waveforms emitted by those accelerated electrons and hence reduced Terahertz power. Decoherence here means that the emitted waveforms from the accelerated charge do not add or combine constructively, i.e. no constructive interference.

In general, electron-electron (or more generally carrier-carrier) scattering is the dominant mechanism at low optical fluences, leading to low photogenerated carrier densities. The design rule above ensures that the length of the electron trajectory s is maximised before scattering off the next adjacent electron located λ away. This is shown schematically in Figure 19. In Figure 19, the direction of THz beam (the emitted beam k_{THz}) is into the page and the magnetic field B is perpendicular and out of the page. The plane of the cyclotron orbit is within the plane of the page.

Figure 20 illustrates the calculated cyclotron radius for values of magnetic field (2T, 4T, 6T and 8T) against optical fluence (solid lines). The mean free path for an optical fluence of 20 nJ/cm^2 , is shown as a weak dotted line.

For an optical fluence of 20 nJ/cm^2 , the intersection of the $\lambda(n)$ vs. n (weak dotted line) and $r(n)$ vs. n (solid lines) suggests that $B=6\text{T}$ is the optimal field, e.g. compromise between reducing electron-electron scattering and thereby maximising power with higher field (hence longer mean free path s) and the practicalities and cost of high magnetic fields.

Figure 21 shows a plot of THz radiation from (100) GaAs measured by a bolometer as a function of the applied magnetic field ($T=200\text{K}$). Circles, triangles and dashed line represent TE, TM-polarised and total emitted power respectively. Crosses are rescaled EOS data (THz field amplitude squared). Solid line is a fit to TE data (circles) with equation (3).

It is often desirable to use a high fluence as, under many types of conditions this will give the highest output power. However, in the high fluence regime, screening of the surface field becomes the dominant mechanism, and the term E_{surf} is dramatically reduced. This means that the efficiency of the source reduces even though the power of the emitted beam increases with the power of the input beam.

The effect of fluence on surface field is illustrated in Figure 22, where the surface field is plotted as a function of depth into the semiconductor from the surface of the sample. The plots were done using a Monte Carlo simulation. The results suggest that in the high fluence limit, screening of the surface field is reduced - and THz power enhanced - with the application of magnetic field. The results suggest that this is valid for time scales from $t=0$ to $t=2\text{ps}$, where $t=0$ is when the Terahertz pulse is received at the detector.

Figure 23 is a plot of the values of the input beam fluence where the fluence crosses from the low regime to the high regime for 5 different magnetic field values (0T, 2T, 4T, 6T and 8T).

This data was found to fit the general exponential function:

$$F=F_0+A\exp(B/t)$$

where F is the fluence of the input beam, B is the magnetic field and F_0 , A and t are fitting parameters. In this particular example, $F_0=70$, $A=56$ and $t=5.7$.

Thus, the boundary between the low and high fluence regimes increases exponentially with increasing magnetic field.

The fluence measurements were taken from the data of Figure 18 where the experimentally measured THz power drops approximately 10% below the linear fit of (1) to the low fluence data. Thus, when dealing with high fluences, it is desirable to

choose a magnetic field such that the source is on the boundary between the low and high fluence limits. Similarly, the optical fluence can be adjusted for a given magnetic field so that it lies on the line of Figure 23.

By way of example, Figure 23 shows the optimal magnetic field ($B=4.7\text{T}$) for a set laser fluence of 200nJ/cm^2 .

CLAIMS:

1. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation, the source being subjected to a magnetic field wherein the free carrier concentration of the frequency conversion member and the applied magnetic field is configured such that the cyclotron diameter of the free carriers of the frequency conversion member is within 30% of their scattering length.
2. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam having a frequency different to that of the emitted beam of radiation, the source being subjected to a magnetic field, the magnetic field and fluence of the input beam being configured to minimise the screening effect of free carriers in the frequency conversion member.
3. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted beam, the frequency conversion member comprises a magnetic material dopant.
4. A radiation source according to claim 3, wherein the dopant is Mn.
5. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to being irradiated with an input beam with a frequency different to that of the emitted beam, the source being subjected to a magnetic field, the source further comprising means for applying an electric field at the surface of the frequency conversion member which is irradiated by the input beam.

6. A radiation source according to claim 5, wherein the means for applying an electric field comprise a pair of Ohmic contacts provided to the frequency conversion member and means for applying a potential difference across said Ohmic contacts.
7. A radiation source according to claim 5, wherein the Ohmic contacts have a substantially triangular shape such that the contacts taper towards one another.
8. A radiation source according to claim 5, wherein the means for applying a field comprises a Schottky gate provided on the surface of the frequency conversion member which is irradiated by the input beam.
9. A radiation source according to any preceding claim, wherein the input beam is circularly or elliptically polarised.
10. A radiation source according to any preceding claim, wherein the magnetic field has a component parallel to that of the emitted beam.
11. A radiation source according to any preceding claim, wherein the emitted beam is produced by reflection of the input beam off a surface of the frequency conversion member.
12. A radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation, the source being subjected to a magnetic field which has a component parallel to that of the emitted beam of radiation, the emitted beam of radiation being produced by reflecting the input beam off a surface of the frequency conversion member.
13. A radiation source according to any preceding claim, wherein the magnetic field is oriented parallel to the emitted beam.

14. A radiation source according to any preceding claim, wherein the magnetic field is oriented at an angle of at most 20° to the emitted beam.
15. A radiation source according to any preceding claim, wherein the frequency conversion member is selected from InAs, InSb and GaAs.
16. A radiation source according to any preceding claim, configured such that the angle between the input beam and the surface normal of the frequency conversion member is substantially the Brewster angle
17. A radiation source according to any preceding claim, wherein the frequency conversion member is subjected to a magnetic field of at least 2T.
18. A radiation source according to any preceding claim, the source further comprising a magnet to apply the said magnetic field.
19. A radiation source according to nay preceding claim, wherein the emitted radiation comprises at least one frequency in the ranges from 0.1 THz to 100THz.
20. A radiation source according to any preceding claim, wherein the input beam is a pulsed beam.
21. A method of optimising a radiation source, the radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation,
the method comprising the step of applying a magnetic field to the source, the magnitude of the magnetic field being chosen in order to minimise the screening of the surface field of the frequency conversion member by free carriers in the frequency conversion member for a predetermined fluence of the input beam.

22. A method of optimising a radiation source, the radiation source comprising a frequency conversion member configured to emit a beam of emitted radiation in response to irradiation with an input beam with a frequency different to that of the emitted radiation,

the method comprising the step of applying a magnetic field to the source, the fluence of the input beam being chosen in order to minimise the screening of the surface field of the frequency conversion member by free carriers in the frequency conversion member for a predetermined magnitude of the applied magnetic field.

23. A method according to either of claims 21 or 22, wherein the magnitude of the applied magnetic field or the optical fluence is determined by the steps of:

- a) measuring the power of the emitted beam as a function of optical fluence for at least three values of magnetic field;
- b) fitting the data measured in a) to the relation:

$$P \propto \frac{n^2 B^2}{m^4} x \left[\frac{\cos \theta_M \sin \theta_M}{2\theta_M} + \frac{1}{2} \right], \quad (1)$$

where P is the power of the emitted beam, n is the free carrier concentration, m is the effective mass of the carriers, B is the magnetic field and θ_M is :

$$\theta_M(n, B) = \arccos \left[1 - \frac{1}{2} \left(\frac{\lambda}{r} \right)^2 \right], \quad (2)$$

where λ is the mean free path which is defined as $1/2(n^{-1/3})$ and r is the cyclotron radius;

c) determining the fluence values for the at least three values of magnetic field where with increasing fluence the measured power starts to diverge from the function of step b); and

d) fitting an exponential function to the at least three values determined in point c) such that the optimum fluence can be determined for a given magnetic field or an optimum magnetic field can be determined for a given fluence.

24. A radiation source as substantially hereinbefore described with reference to any of the accompanying drawings.
25. A method of optimising a radiation source as substantially hereinbefore described with reference to any of the accompanying drawings.

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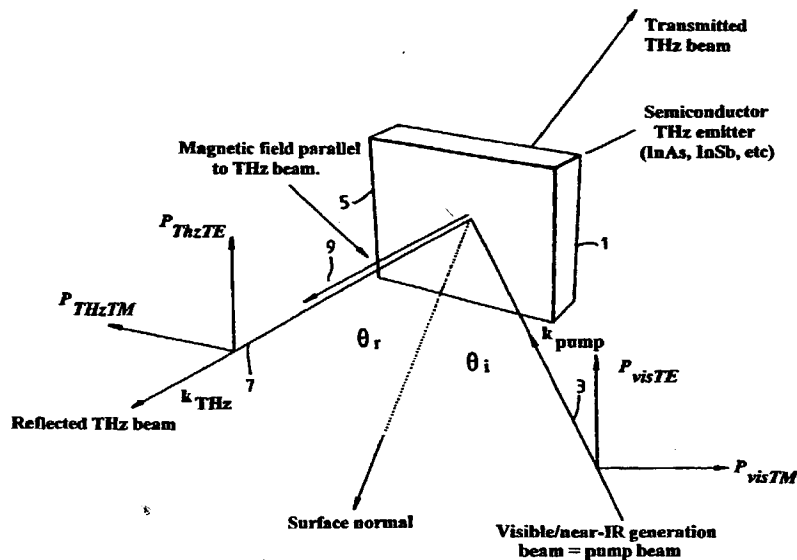
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(54) Title: A RADIATION SOURCE



(57) Abstract: A radiation source comprising a frequency conversion member (1) configured to emit a beam of emitted radiation (7) with at least one frequency in the range from 0.1 THz to 100 THz, in response to irradiation with an input beam (3) with a frequency different to that of the emitted radiation (7), the source being subjected to a magnetic field (9) which has a component parallel to that of the emitted beam of radiation (7). The radiation source may be optimised by using both the fluence of the input beam and the magnetic field or may comprise a magnetically doped frequency conversion member or also have means for applying an electric field.

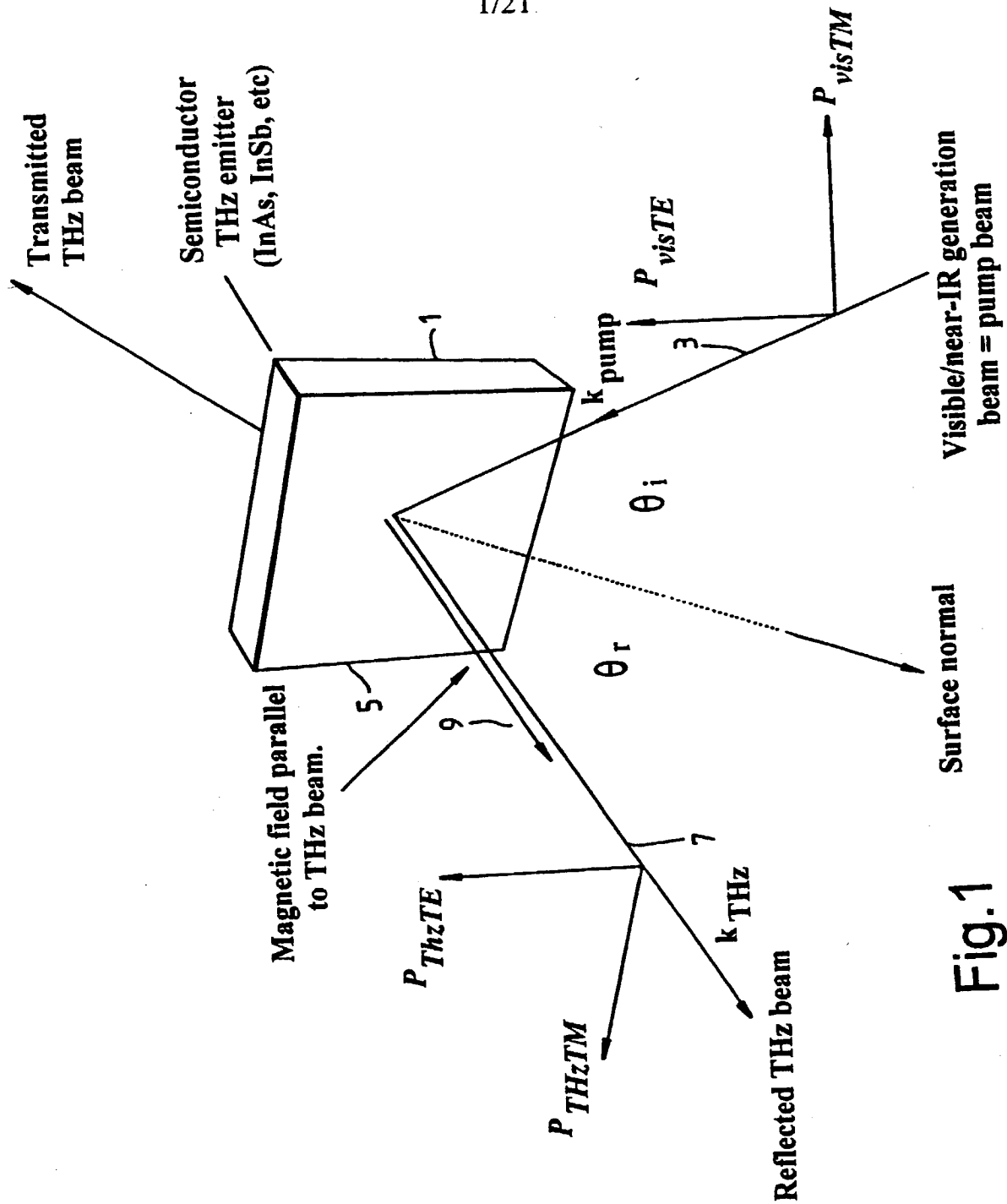


Fig.1

2/21

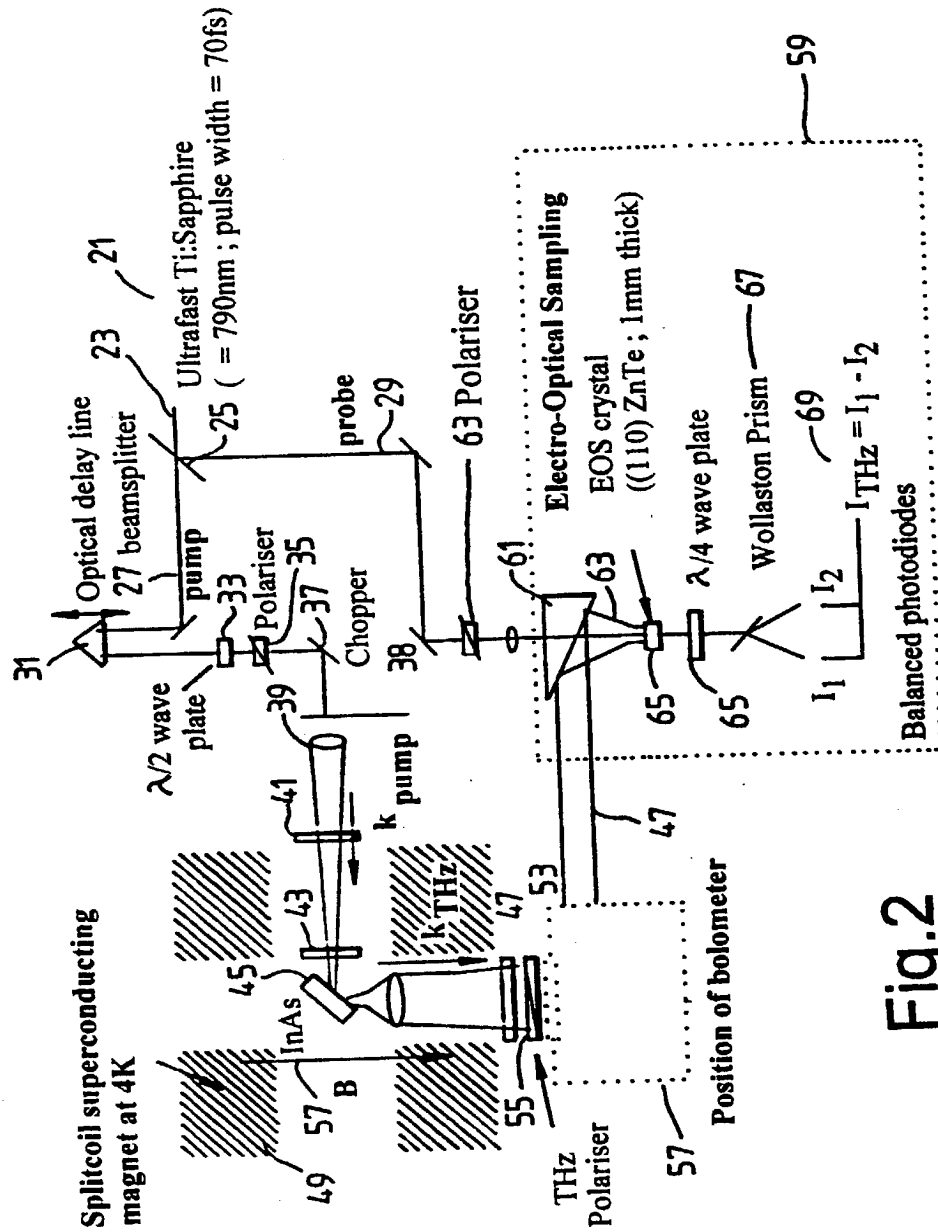


Fig.2

3/21

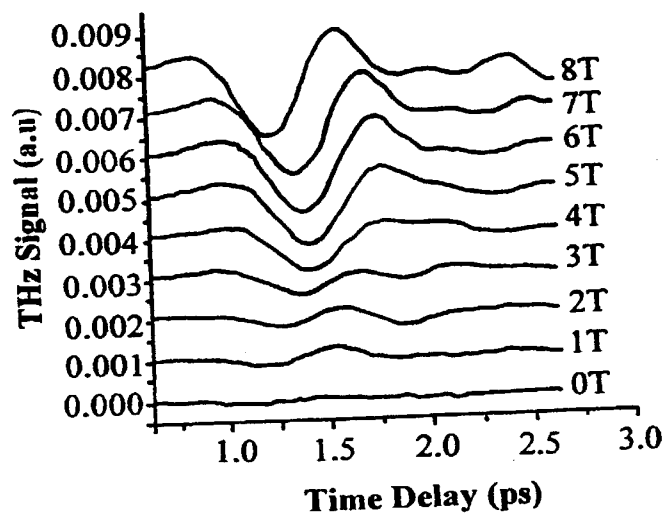
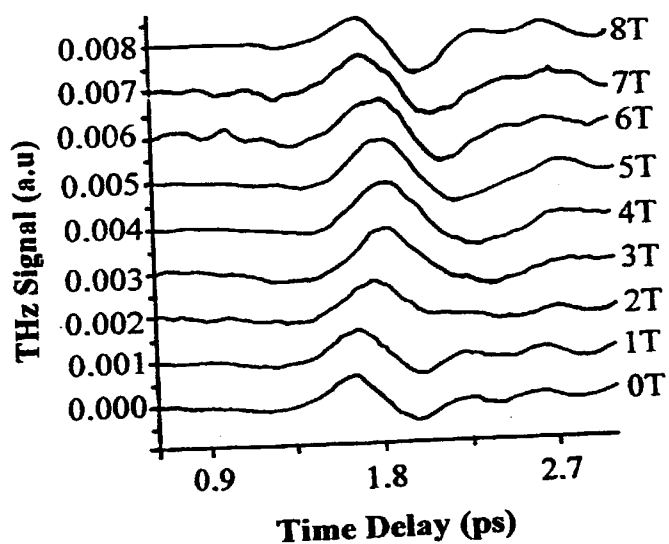


Fig.3

4/21

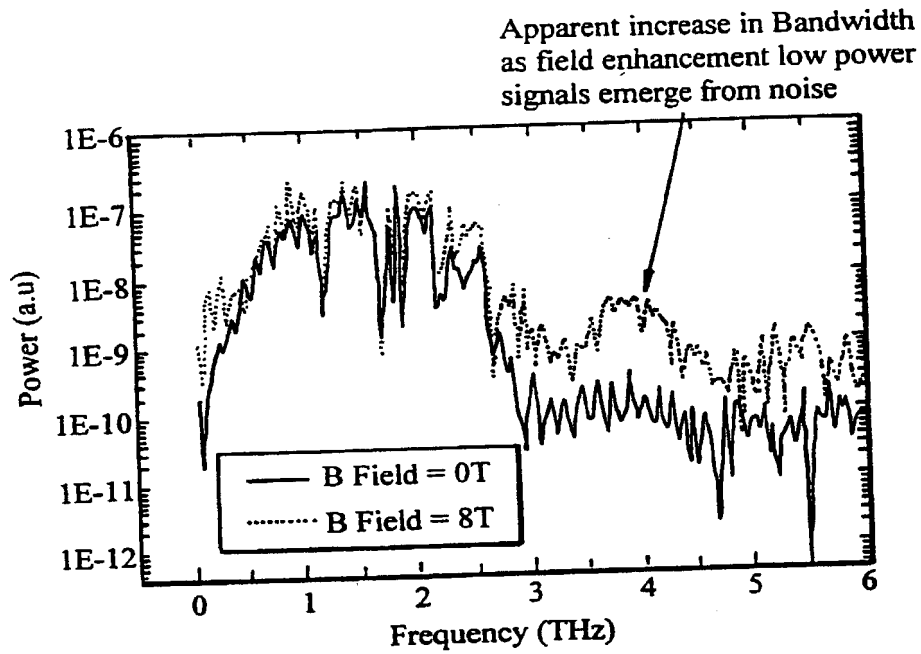


Fig.4

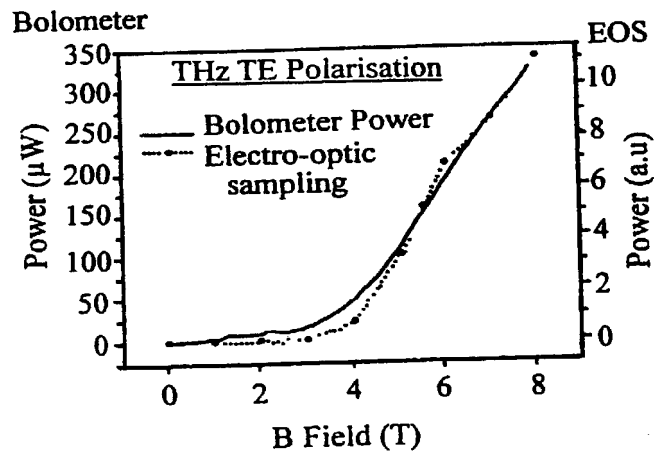


Fig.5

5/21

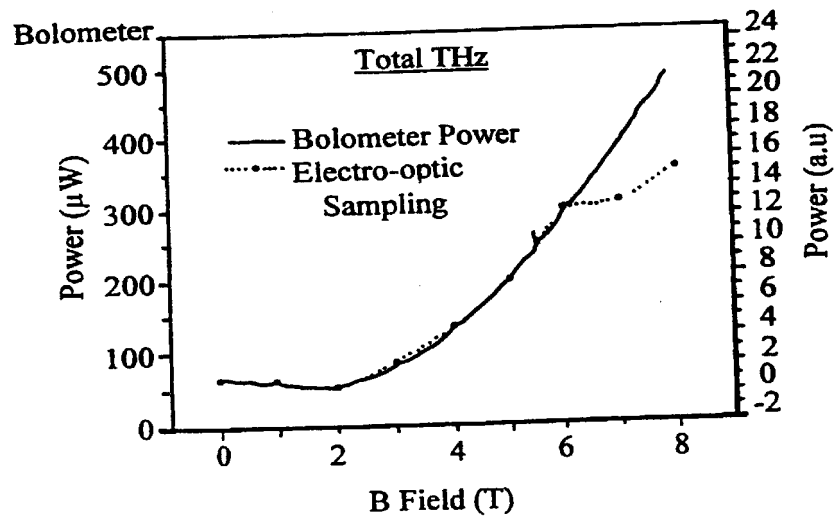
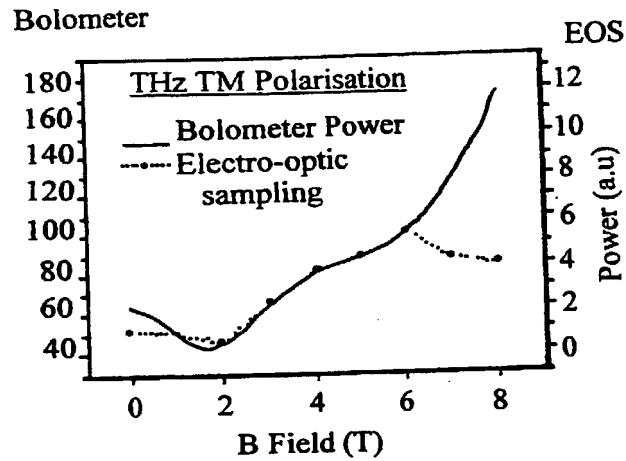


Fig. 5(cont'd)

6/21

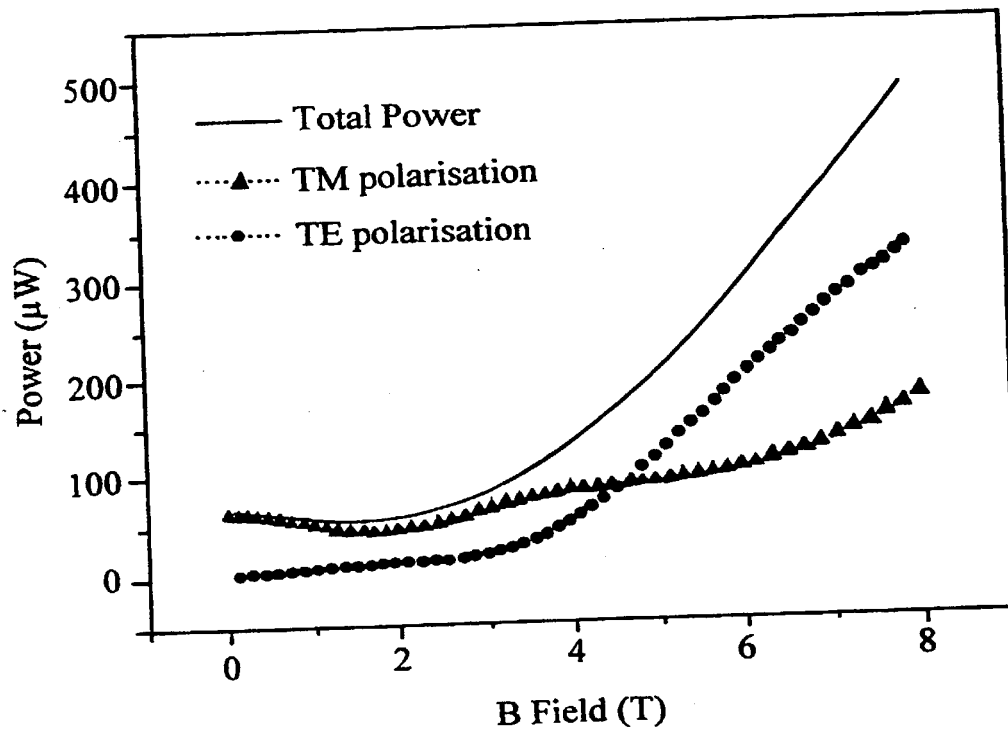


Fig.6

7/21

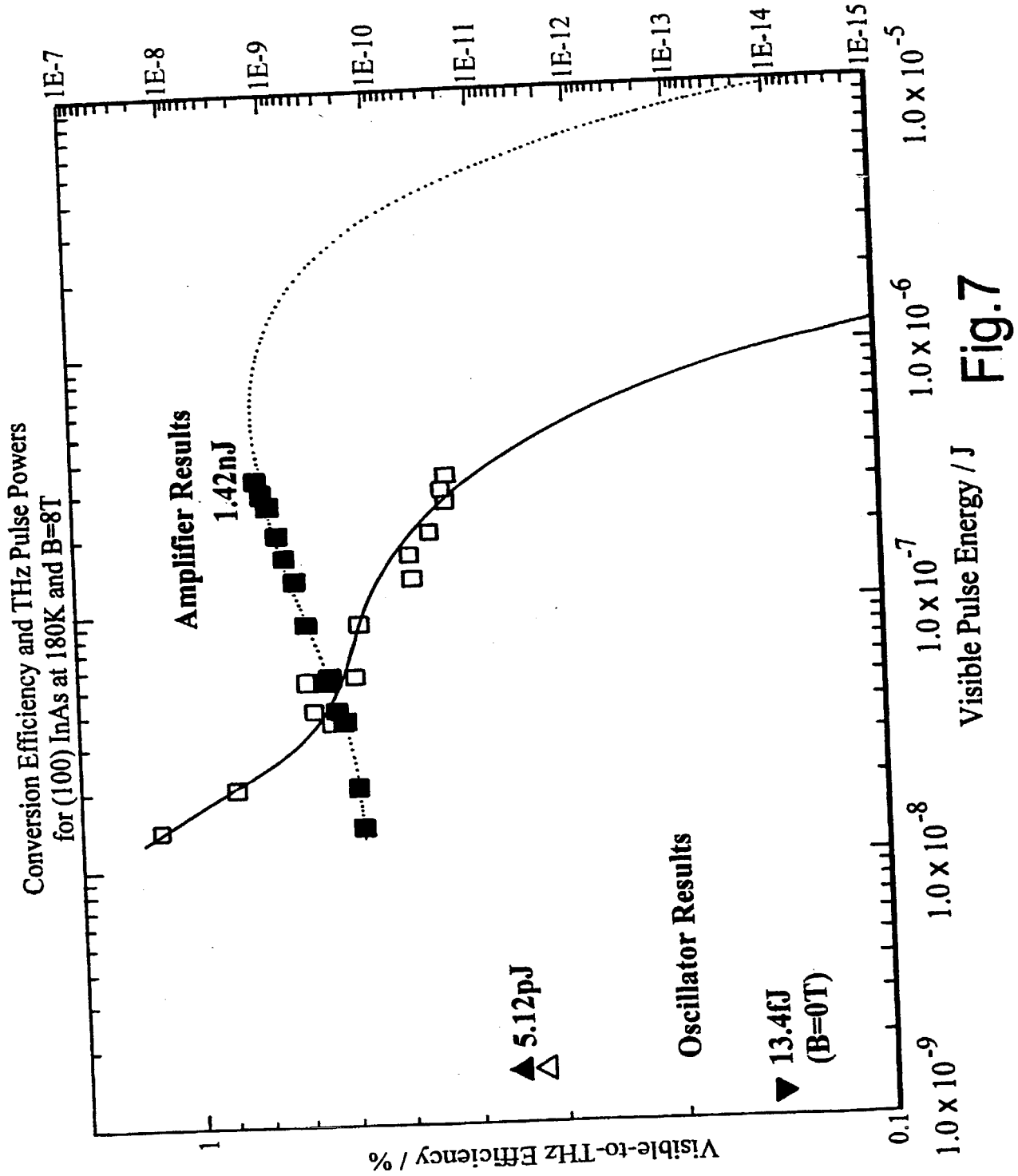


Fig.7

8/21

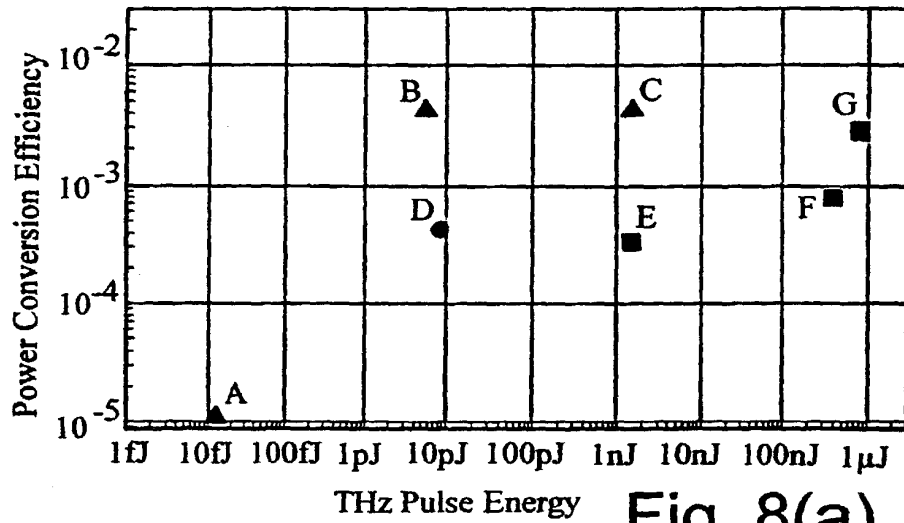


Fig. 8(a)

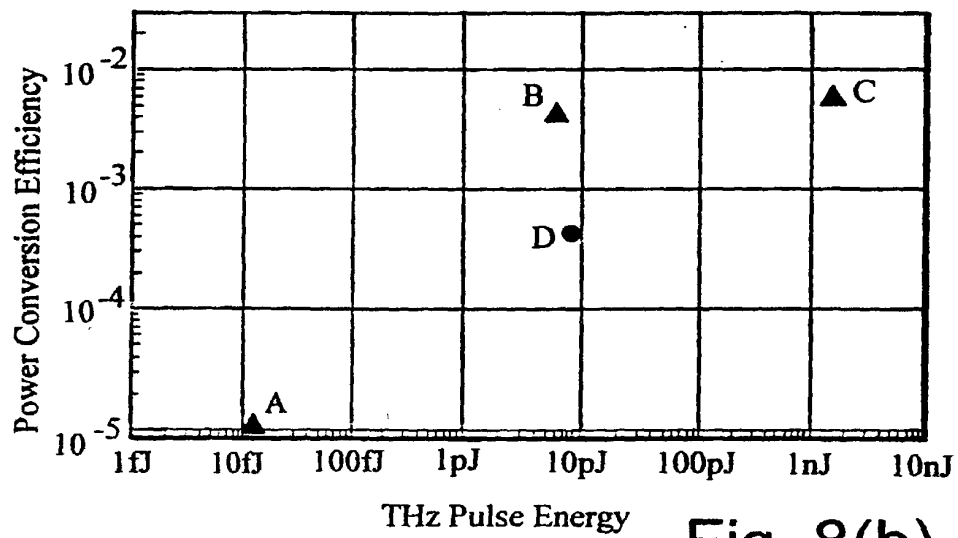
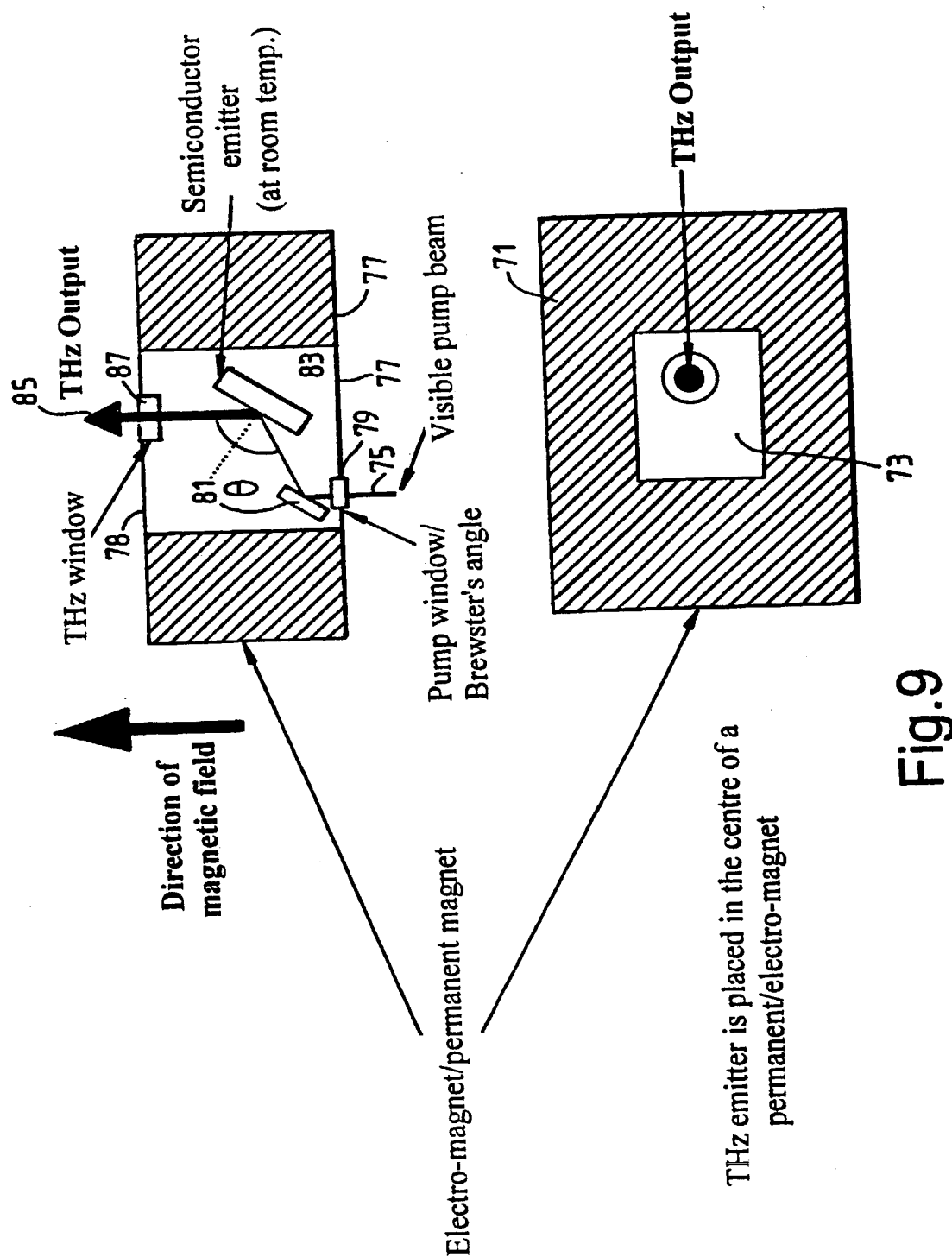


Fig. 8(b)

9/21



10/21

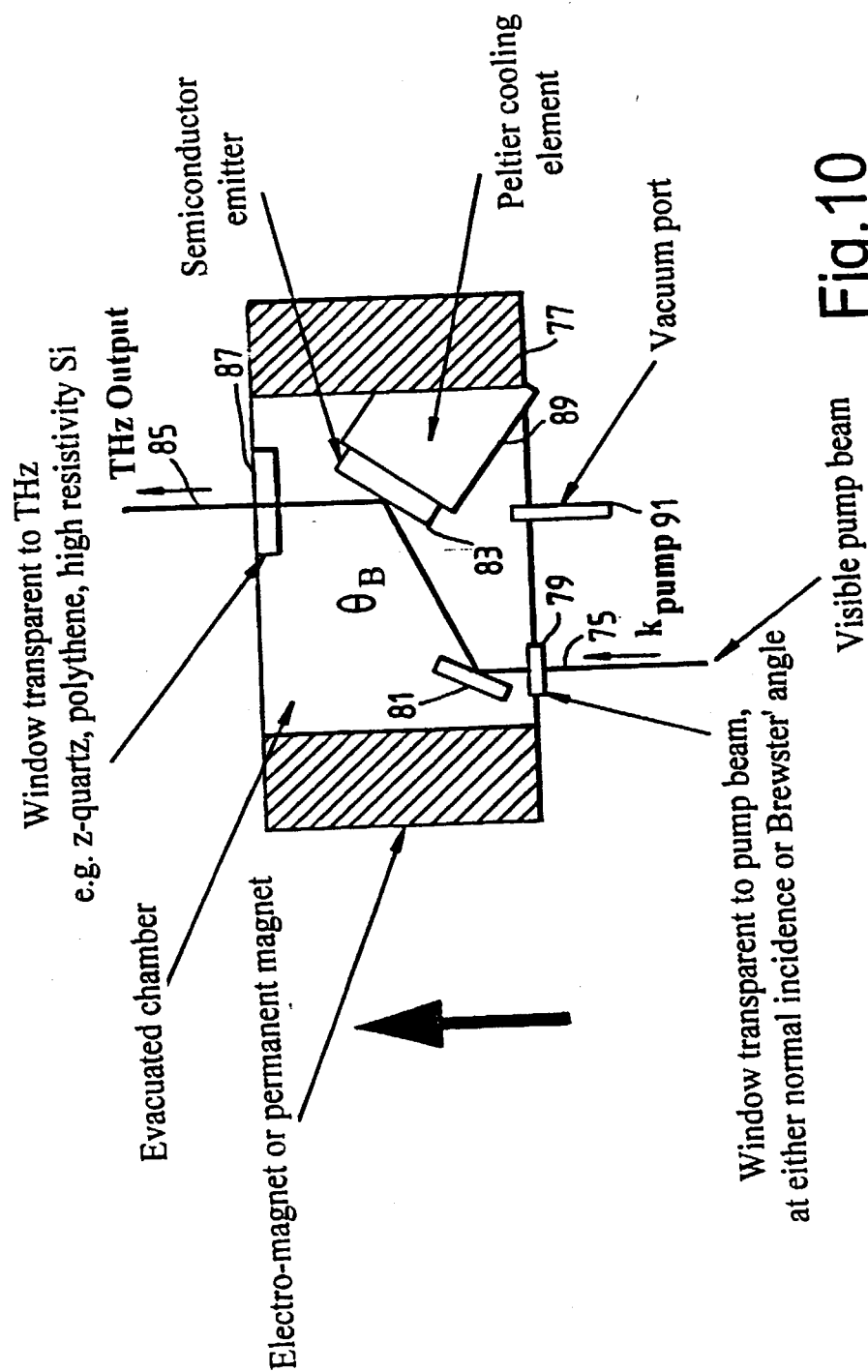


Fig.10

11/21

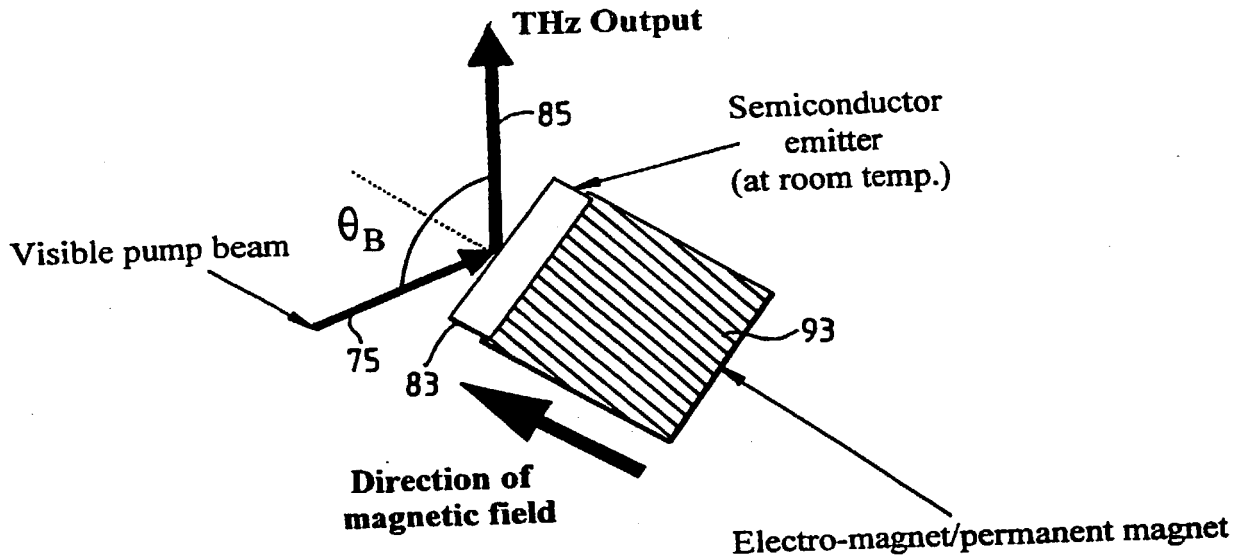


Fig.11

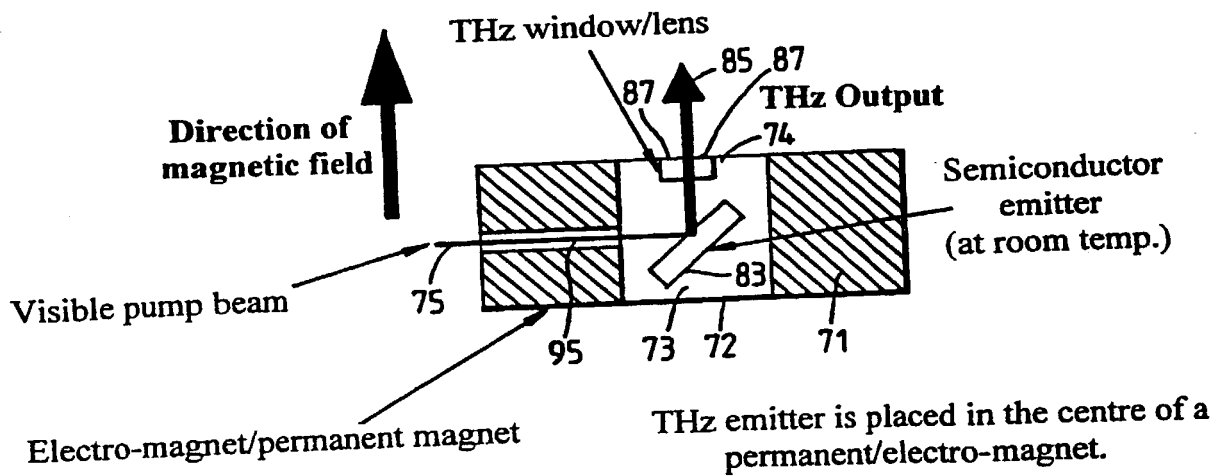


Fig.12

12/21

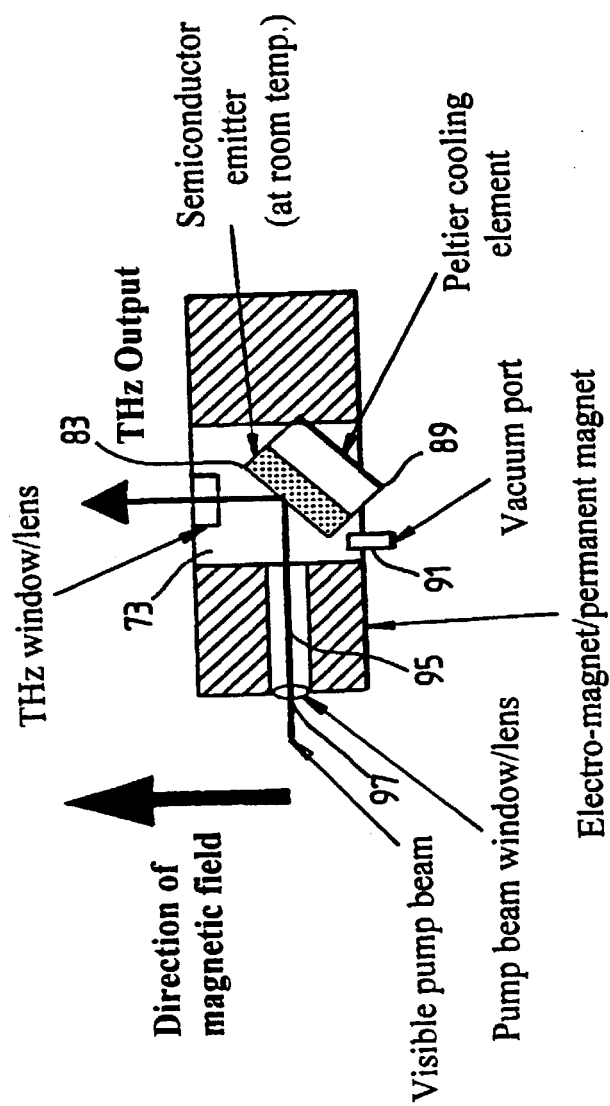


Fig.13

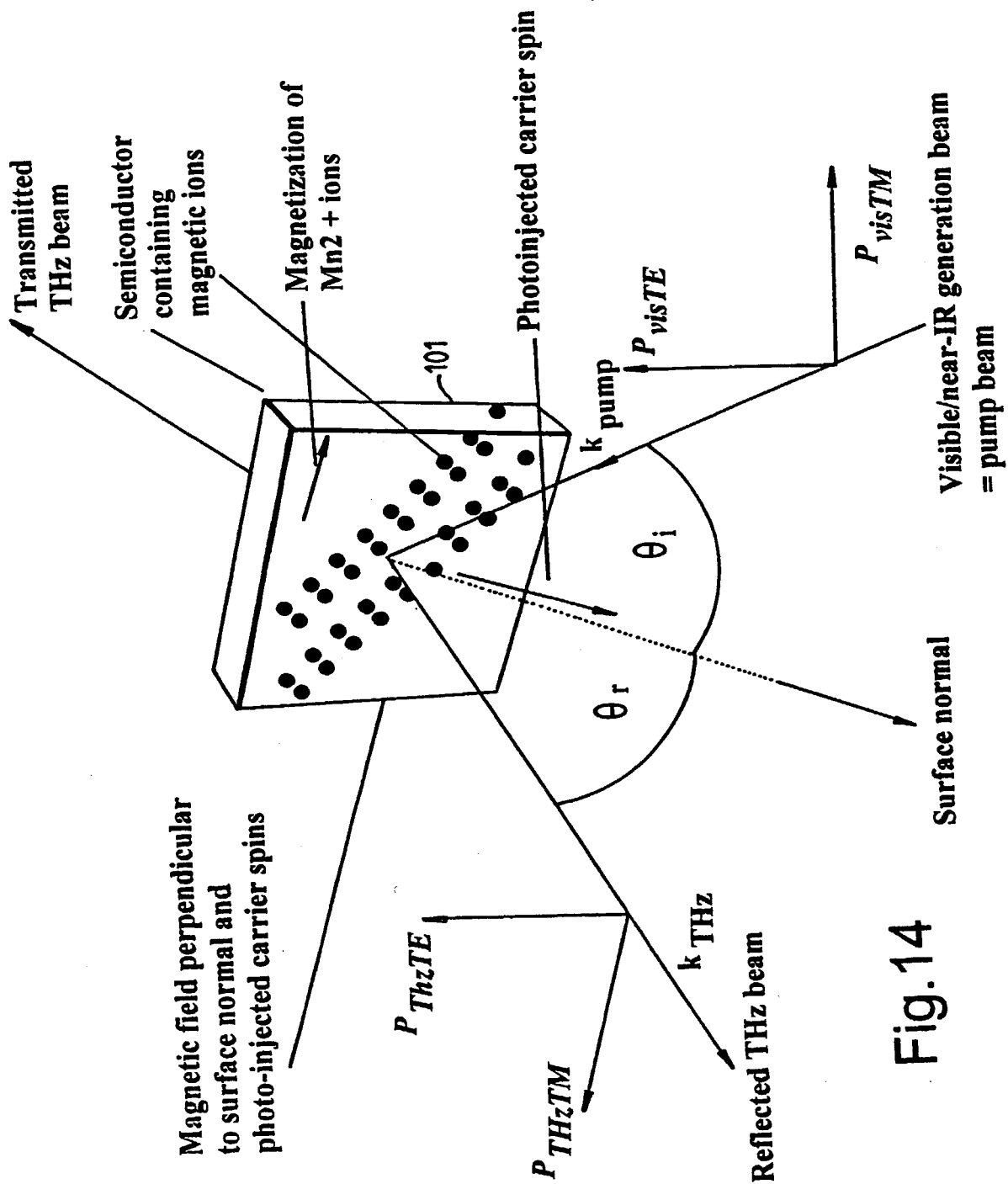


Fig. 14

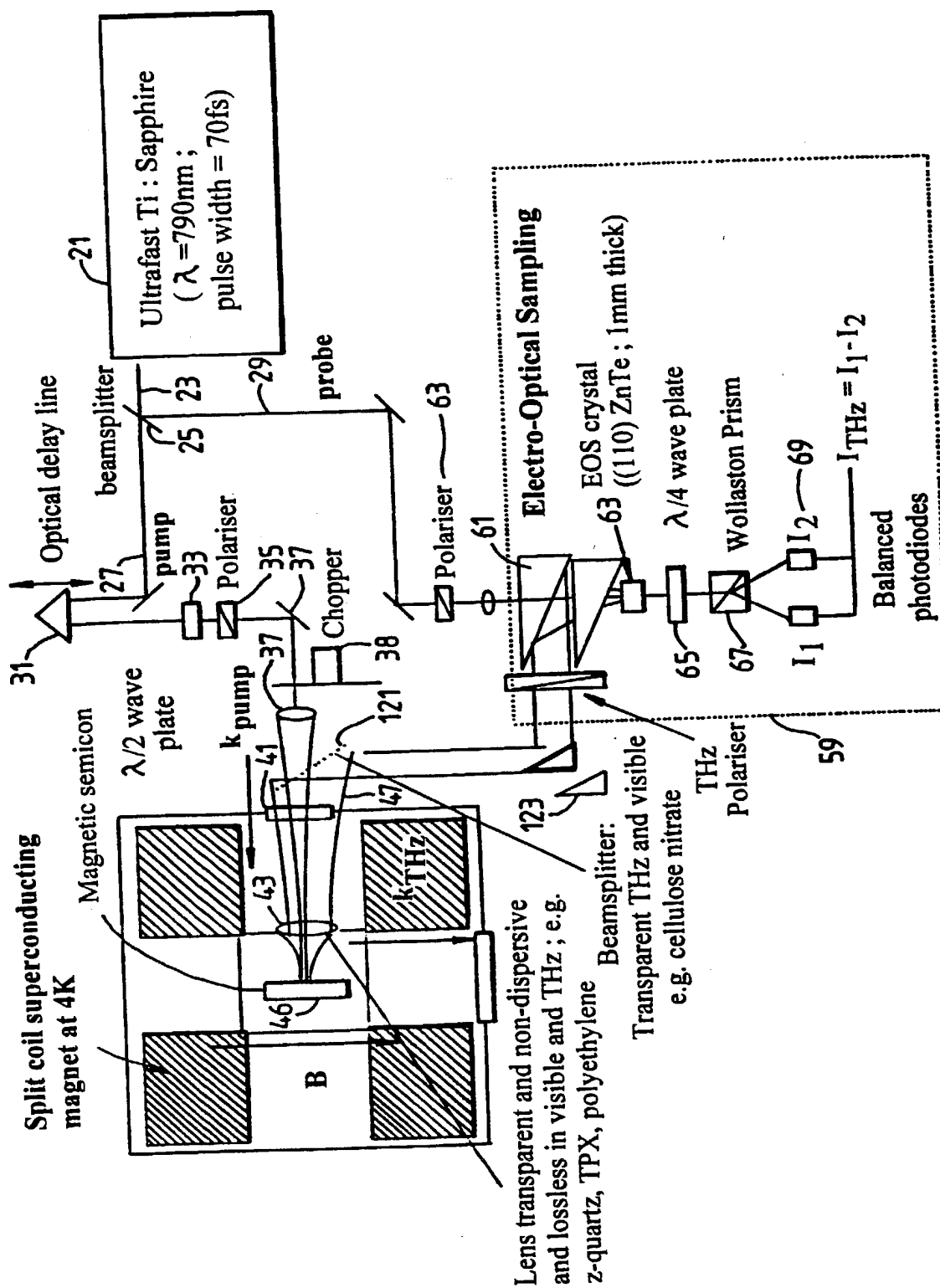


Fig. 15

15/21

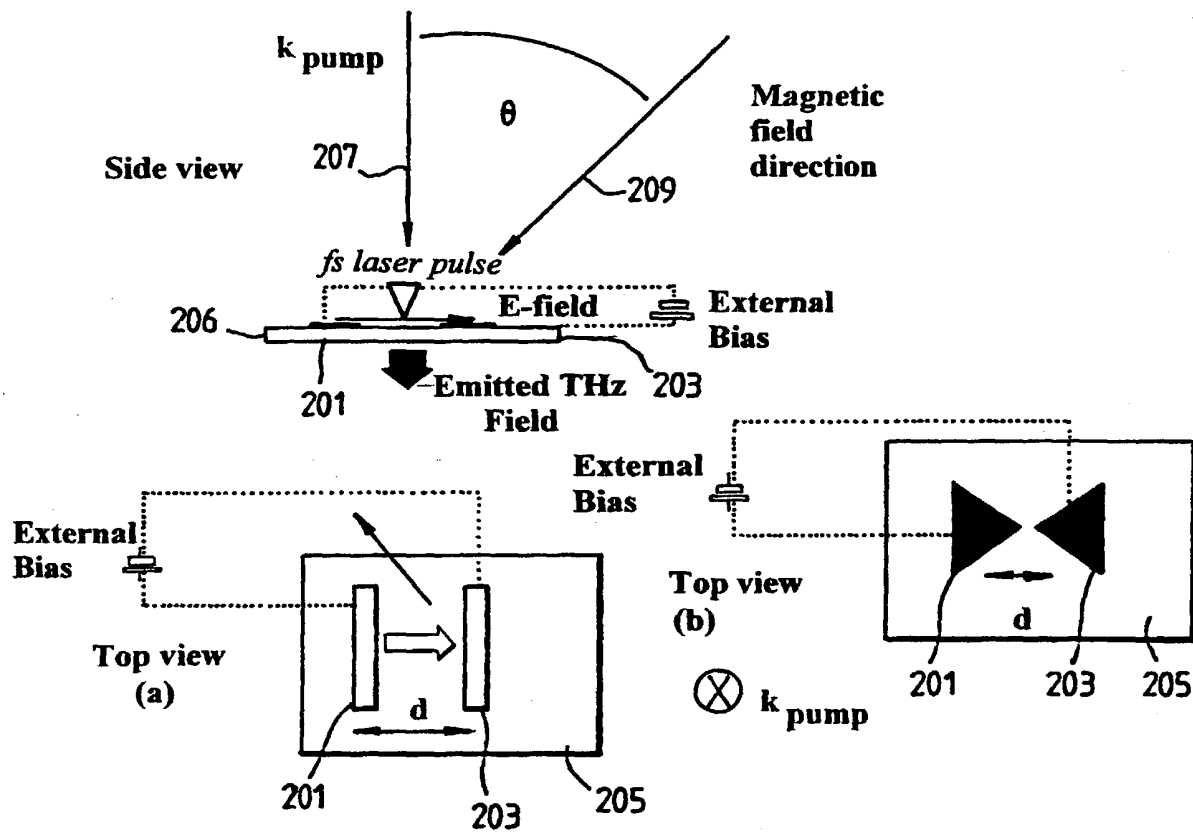


Fig.16

16/21

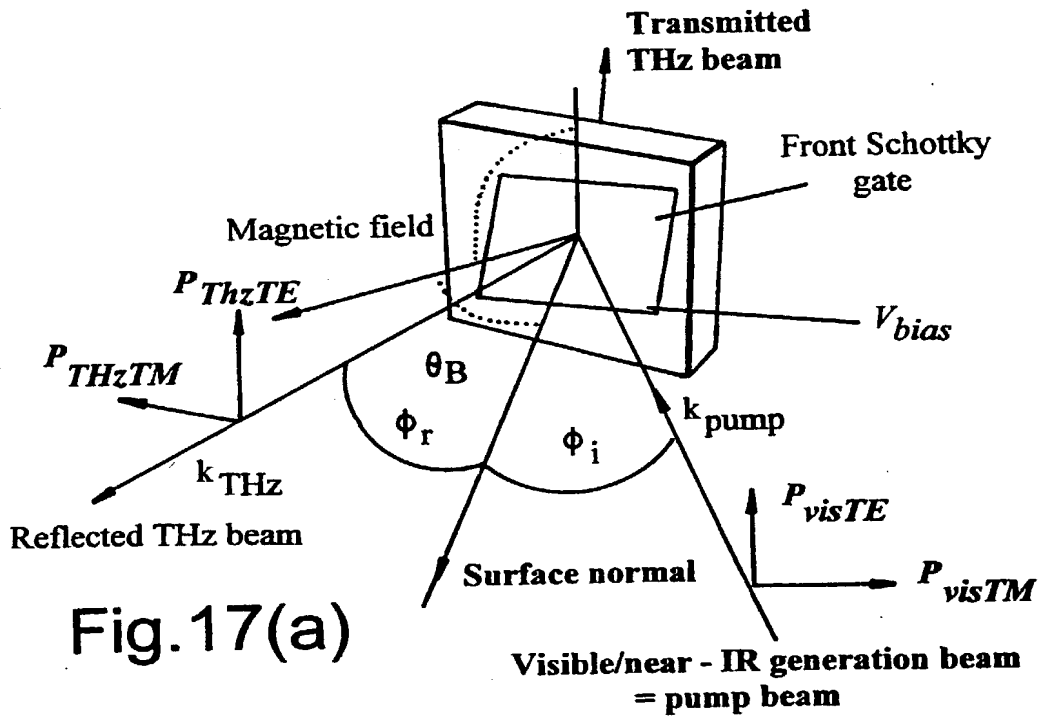


Fig.17(a)

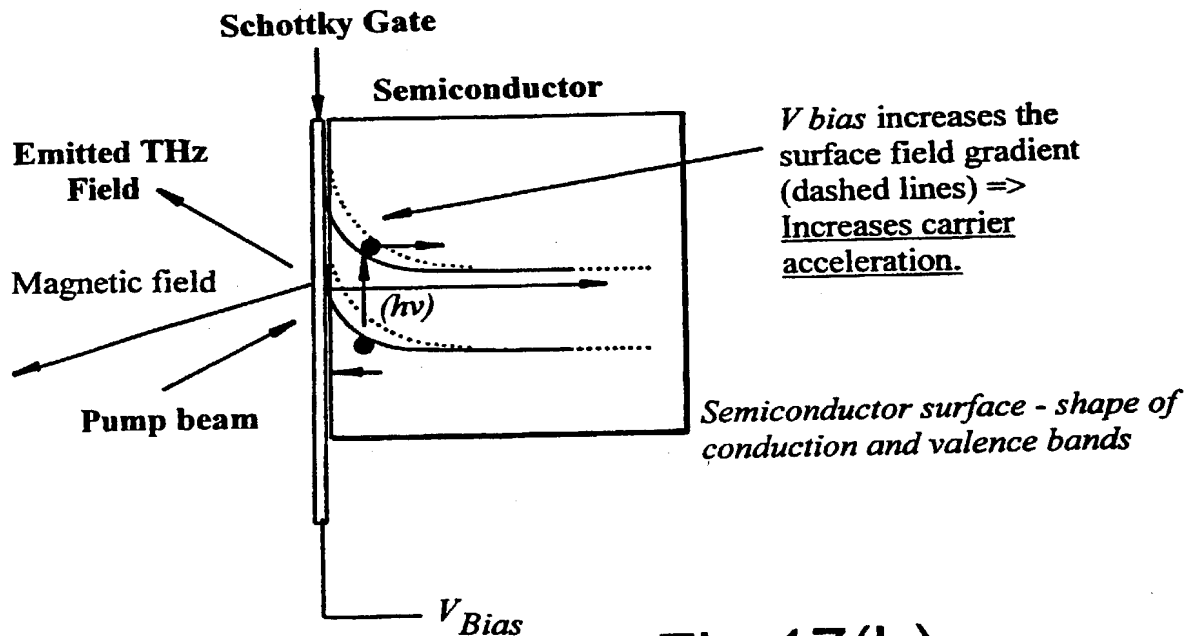


Fig.17(b)

17/21

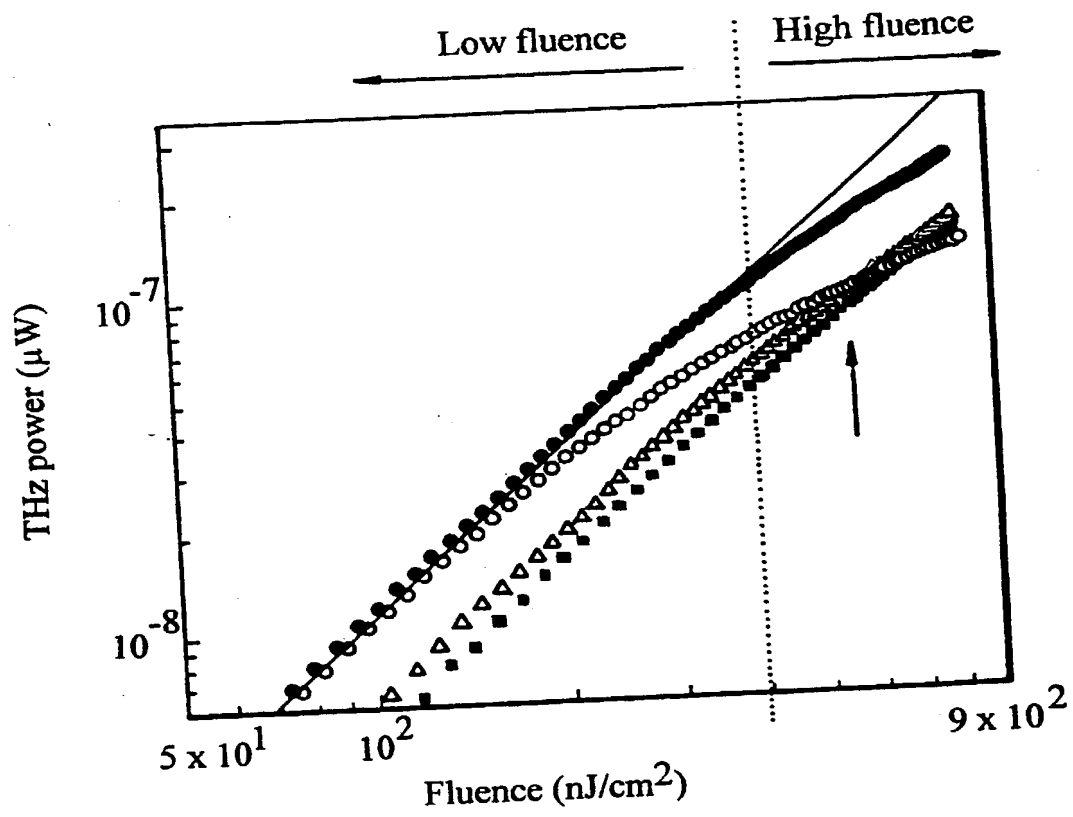


Fig. 18

18/21

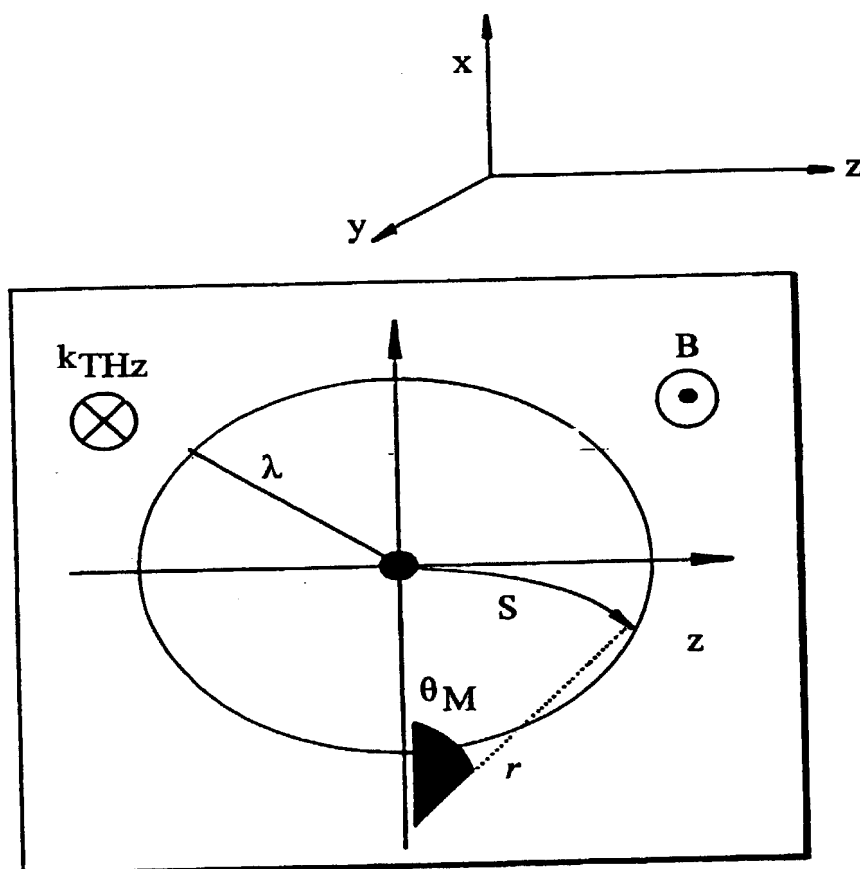


Fig. 19

19/21

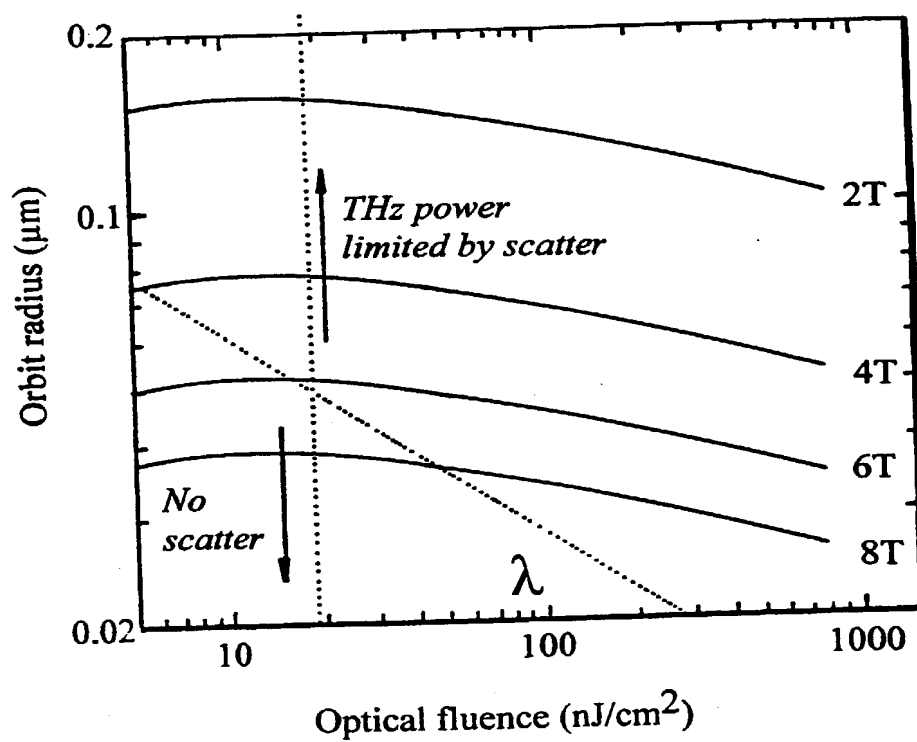


Fig. 20

20/21

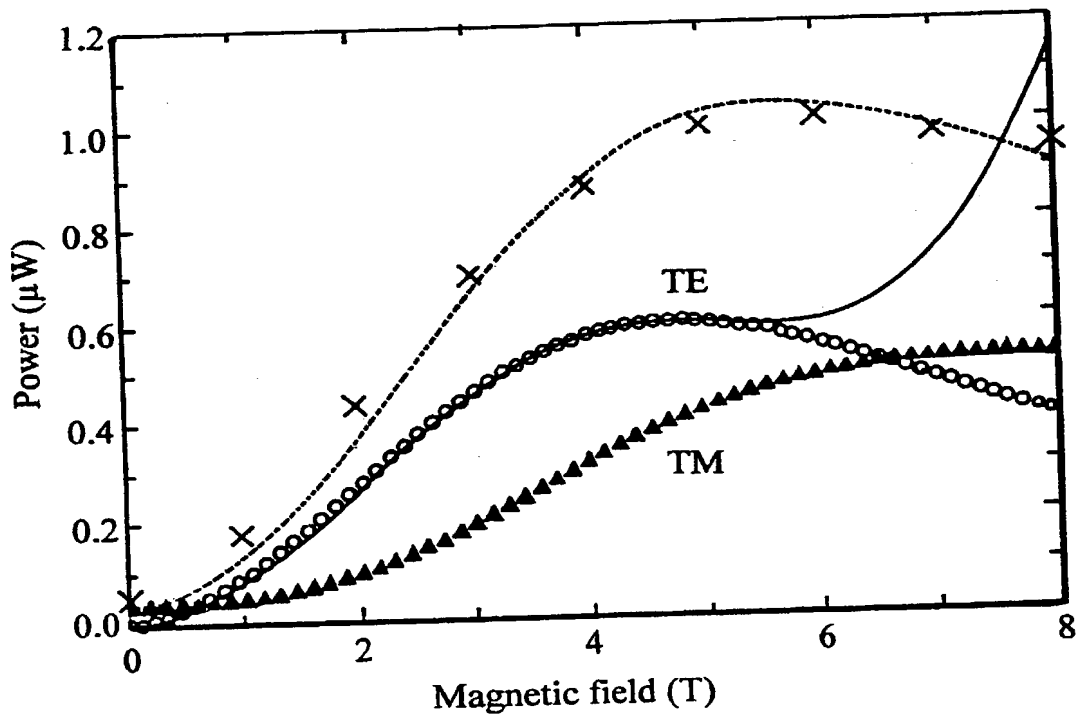


Fig. 21

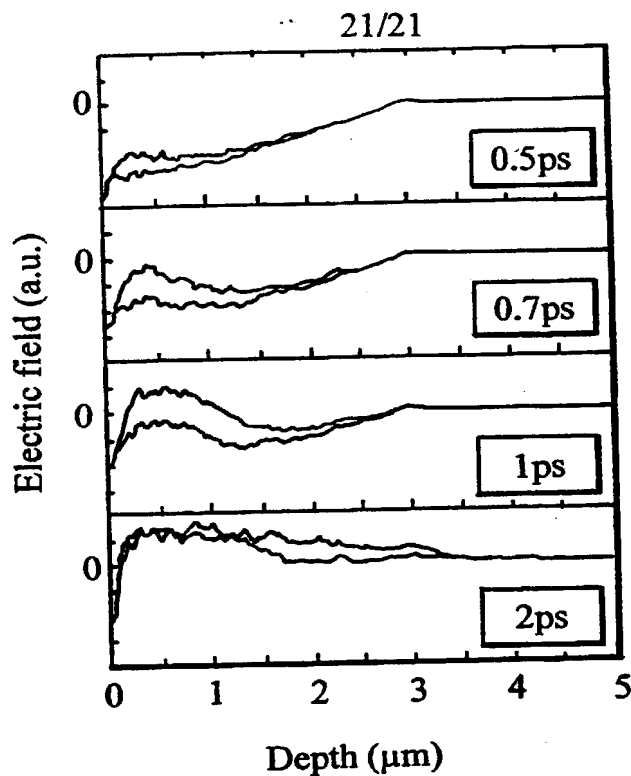


Fig. 22

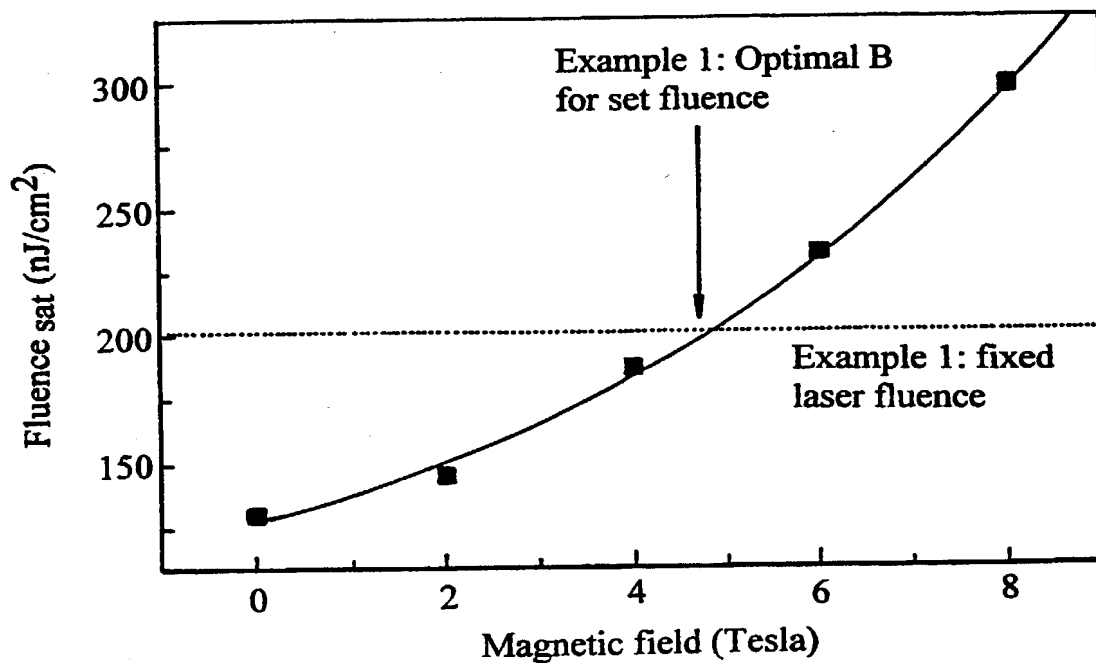


Fig. 23

| UNITED STATES OF AMERICA COMBINED DECLARATION AND POWER OF ATTORNEY FOR PATENT APPLICATION | | OFGS FILE NO. P/25-277 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--------------------------------------|--|---|---------|--------------------|--------------------------------------|---|---------------|-----------|-------------------|---|--|--|--|--|--|--|--|--|-------------------------------------|--------------------------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|-------------------|--|--|---|--|---|--|--|--|---|--|---|-------------------|--|--|---|--|---|--|--|--|
| <p>As a below named inventor, I hereby declare that my residence, post office address and citizenship are as stated below next to my name; that I verily believe that I am the original, first and sole inventor (if only one name is listed below) or a joint inventor (if plural inventors are named) of the subject matter which is claimed and for which a patent is sought on the invention entitled:</p> <p>A RADIATION SOURCE</p> <p>the specification of which is attached hereto, unless the following box is checked:</p> <p><input checked="" type="checkbox"/> was filed on <u>March 27, 2002</u> as United States patent Application Number or PCT International patent application number <u>10/089,488</u> and was amended on _____ (if any).</p> <p>I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.</p> <p>I acknowledge the duty to disclose all information known to be material to patentability in accordance with Title 37, Code of Federal Regulations, §1.56.</p> <p>I hereby claim priority benefits under Title 35, United States Code §119 of any foreign application(s) for patent or inventor's certificate or United States provisional application(s) listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:</p> <p>Prior Foreign or Provisional Application(s)</p> <table border="1"> <thead> <tr> <th>COUNTRY</th> <th>APPLICATION NUMBER</th> <th>DATE OF FILING (day, month, year)</th> <th>PRIORITY CLAIMED UNDER 35 U.S.C. 119</th> </tr> </thead> <tbody> <tr> <td>Great Britain</td> <td>9922859.5</td> <td>27 September 1999</td> <td>YES <input checked="" type="checkbox"/> NO <input type="checkbox"/></td> </tr> <tr> <td></td> <td></td> <td></td> <td>YES <input type="checkbox"/> NO <input type="checkbox"/></td> </tr> <tr> <td></td> <td></td> <td></td> <td>YES <input type="checkbox"/> NO <input type="checkbox"/></td> </tr> </tbody> </table> <p>I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, §1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application.</p> <table border="1"> <thead> <tr> <th>UNITED STATES APPLICATION NUMBER</th> <th>DATE OF FILING (day, month, year)</th> <th>STATUS (patented, pending, abandoned)</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> </tbody> </table> <p>I hereby appoint customer no. 2352 OSTROLENK, FABER, GERB & SOFFEN, LLP, and the members of the firm, Samuel H. Weiner - Reg. No. 18,510; Jerome M. Berliner - Reg. No. 18,653; Robert C. Faber - Reg. No. 24,322; Max Moskowitz - Reg. No. 30,576; James A. Finder - Reg. No. 30,173; William O. Gray, III - Reg. No. 30,944; Louis C. Dujmich - Reg. No. 30,625, and Douglas A. Miro - Reg. No. 31,643, as attorneys with full power of substitution and revocation to prosecute this application, to transact all business in the Patent & Trademark Office connected therewith and to receive all correspondence.</p> <p>SEND CORRESPONDENCE TO: OSTROLENK, FABER, GERB & SOFFEN, LLP 1180 AVENUE OF THE AMERICAS NEW YORK, NEW YORK 10036-8403 CUSTOMER NO. 2352</p> <p>DIRECT TELEPHONE CALLS TO: (212) 382-0700</p> <p>I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.</p> <table border="1"> <tr> <td colspan="2">FULL NAME OF SOLE OR FIRST INVENTOR Donald Dominic ARNONE</td> <td>INVENTOR'S SIGNATURE <i>Donald Dominic Arnone</i></td> <td>DATE 07 Aug 02</td> </tr> <tr> <td colspan="2">RESIDENCE (City and either State or Foreign Country) Cambridge, CB4 0WG, United Kingdom GBX</td> <td colspan="2">COUNTRY OF CITIZENSHIP United States</td> </tr> <tr> <td colspan="4">POST OFFICE ADDRESS c/o TeraView Limited, 302/304 Cambridge Science Park, Milton Road, Cambridge, CB4 0WG, United Kingdom</td> </tr> <tr> <td colspan="2">FULL NAME OF SECOND JOINT INVENTOR (if any) Craig Michael CIESLA</td> <td>INVENTOR'S SIGNATURE <i>Craig Michael Ciesla</i></td> <td>DATE Aug-01-02</td> </tr> <tr> <td colspan="2">RESIDENCE (City and either State or Foreign Country) Cambridge, CB4 0WG, United Kingdom GBX</td> <td colspan="2">COUNTRY OF CITIZENSHIP Great Britain</td> </tr> <tr> <td colspan="4">POST OFFICE ADDRESS c/o TeraView Limited, 302/304 Cambridge Science Park, Milton Road, Cambridge, CB4 0WG, United Kingdom</td> </tr> </table> | | | | COUNTRY | APPLICATION NUMBER | DATE OF FILING (day, month, year) | PRIORITY CLAIMED UNDER 35 U.S.C. 119 | Great Britain | 9922859.5 | 27 September 1999 | YES <input checked="" type="checkbox"/> NO <input type="checkbox"/> | | | | YES <input type="checkbox"/> NO <input type="checkbox"/> | | | | YES <input type="checkbox"/> NO <input type="checkbox"/> | UNITED STATES APPLICATION NUMBER | DATE OF FILING (day, month, year) | STATUS (patented, pending, abandoned) | | | | | | | | | | FULL NAME OF SOLE OR FIRST INVENTOR Donald Dominic ARNONE | | INVENTOR'S SIGNATURE <i>Donald Dominic Arnone</i> | DATE 07 Aug 02 | RESIDENCE (City and either State or Foreign Country) Cambridge, CB4 0WG, United Kingdom GBX | | COUNTRY OF CITIZENSHIP United States | | POST OFFICE ADDRESS c/o TeraView Limited, 302/304 Cambridge Science Park, Milton Road, Cambridge, CB4 0WG, United Kingdom | | | | FULL NAME OF SECOND JOINT INVENTOR (if any) Craig Michael CIESLA | | INVENTOR'S SIGNATURE <i>Craig Michael Ciesla</i> | DATE Aug-01-02 | RESIDENCE (City and either State or Foreign Country) Cambridge, CB4 0WG, United Kingdom GBX | | COUNTRY OF CITIZENSHIP Great Britain | | POST OFFICE ADDRESS c/o TeraView Limited, 302/304 Cambridge Science Park, Milton Road, Cambridge, CB4 0WG, United Kingdom | | | |
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| Great Britain | 9922859.5 | 27 September 1999 | YES <input checked="" type="checkbox"/> NO <input type="checkbox"/> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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